

CRC VOLATILITY PROGRAM ON THE EFFECT OF OXYGENATED FUELS AND ALTITUDE ON COLD-START DRIVEABILITY AT LOW AMBIENT TEMPERATURES

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CRC VOLATILITY PROGRAM ON THE EFFECT OF OXYGENATED FUELS AND ALTITUDE ON COLD-START DRIVEABILITY AT LOW AMBIENT TEMPERATURES (CRC Project No. CM-118-88)

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Prepared by the

1988 Analysis Panel of the CRC Volatility Group

January 1990

Automotive Vehicle Fuel, Lubricant, and Equipment Research Committee

of the

Coordinating Research Council, Inc.

ABSTRACT

The 1988 CRC driveability program investigated the effects of altitude and fuel oxygenates at low ambient temperature upon cold-start driveability with vehicles equipped with various fuel systems. This program was conducted because of the use of gasoline-oxygenate blends to reduce ambient air carbon monoxide levels. The test program was divided into two phases. A high-altitude phase was conducted near Denver, Colorado, from January 11 through February 10, 1988, at an altitude of 5,486 feet; and a low-altitude phase was conducted in Brainerd, Minnesota, from March 4 through March 31, 1988, at an altitude of 1,226 feet. Test temperatures were 10 F to 40 F. Twenty-four vehicles chosen to represent a variety of engines and fuel systems tested twelve test fuels, including hydrocarbon-only fuels, gasoline-ethanol blends, and gasoline-MTBE blends. The altitude change between the two sites was found to have no statistically significant effect on driveability for the overall fleet. Driveability performance decreased statistically significantly with declining ambient temperatures. For the overall fleet, the oxygenate-containing fuels evaluated performed poorer than hydrocarbon-only fuels at a statistically significant level. In the throttle-body-injected and new carbureted vehicle groups, however, only the matched-volatility ethanol blends gave poorer driveability performance than the hydrocarbon-only fuels at a statistically significant level. In port-fuel-injected vehicles, none of the oxygenate-containing fuels gave different performance than the hydrocarbon-only fuels at a statistically significant level. For the old carbureted vehicle group, all the oxygenate blends gave poorer performance than the hydrocarbononly fuels at a statistically significant level. The effect of volatility level was statistically significant; as expected, increasing T_{10} and/or T_{50} gave poorer performance.

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I. INTRODUCTION

The 1988 CRC driveability program investigated the effects of altitude and fuel oxygenates at low ambient temperature upon cold-start driveability with vehicles equipped with carbureted, throttle-body-injected, and port-fuel-injected fuel delivery systems. This program was conducted because of the use of gasoline-oxygenate blends to reduce ambient air carbon monoxide levels. Although several CRC programs have been conducted in recent years to investigate the effect of oxygenated fuels on driveability, there is limited information on the effects of oxygenated blends at altitude. Most of the recent CRC work has concentrated on closed-loop, fuel-injected vehicles. Since Colorado has been at the forefront of the movement to require the use of oxygenated fuels during winter months, and since the Denver area has a high percentage of open-loop vehicles, the test fleet for the 1988 program also included a number of pre-1980 open-loop vehicles.

The test program was divided into two phases: a high-altitude phase was conducted near Denver, Colorado, from January 11 through February 10, 1988, at an altitude of 5,486 feet; and a low-altitude phase was conducted in Brainerd, Minnesota, from March 4 through March 31, 1988, at an altitude of 1,226 feet. Test temperatures were $10^{\circ} F$ to $40^{\circ} F$.

Members of the Data Analysis Panel and participants in the test program are shown in Appendices A and B, respectively. Appendix C outlines the proposed program as approved by the CRC Volatility Group, and Appendix D details the fuel/vehicle assignments for each test day. A preliminary report on the test program, issued in May 1988, is attached to this report as Appendix E.

II. SUMMARY AND CONCLUSIONS

Analysis of the data provided the following conclusions:

- The altitude change between the two sites had no significant effect on driveability. For the fleet, demerits at high altitude were only 5 percent higher than at low altitude.
- Over the range of 10°F to 40°F, the temperature effect for the pre-1980 carbureted vehicles at 363 average total weighted demerits (TWD's) was a decrease of 4.9 TWD's per degree Fahrenheit increase in ambient temperature. The effect for the new model vehicles at an average TWD level of 70 was a decrease of 1.3 TWD's per degree Fahrenheit increase in ambient temperature, which was significantly different from the pre-1980 vehicle effect.

- For the overall fleet, the hydrocarbon-only fuels performed better than the oxygenate-containing fuels at a statistically significant level. The splash-blended ethanol (3.5 wt.% oxygen) and matched-volatility MTBE (2 wt.% oxygen) were not different from each other at a statistically significant level, but were better than the matched-volatility ethanol blends at a statistically significant level. These effects occurred independently of vehicle type.
- The effect of volatility level was significant. As expected, increasing T_{10} and/or T_{50} gave poorer performance. This effect occurred independently of oxygenate.
- Within current-model vehicles, port-fuel-injected vehicles provided the best performance, followed by throttle-body-injected, and carbureted vehicles; however, these differences were not statistically significant.
- The pre-1980 carbureted vehicles gave much poorer performance than current-model carbureted or fuel-injected vehicles. This difference was found to be highly significant.
- Within each vehicle group, large vehicle-to-vehicle variability in performance was found.

The results found in this study are a technical indication of driveability using trained raters. The test was not designed to predict how the statistical significance of any difference found relates to customer perception of the performance of the fuels.

III. TEST VEHICLES

The test fleet is shown in Table I. Fifteen of the vehicles were 1987 or 1988 model years with closed-loop (feedback) fuel metering systems. Included in this group were five port-fuel-injected (PFI), four throttle-body-injected (TBI), and six carbureted vehicles. Of the PFI vehicles, one was turbocharged and another was equipped with a four-valve engine. An additional six vehicles were 1978 or 1979 model years with open-loop metering systems. Throughout the report, the six 1987 or 1988 model-year carbureted vehicles will be referred to as "new" carbureted vehicles, and the 1978 or 1979 vehicles as "old" carbureted vehicles. The three additional vehicles shown in Table I were used to develop rater correction factors. All 1987/1988 vehicles were equipped with air-conditioning, Federal emission control devices, and automatic transmissions.

The PFI vehicles were designated as Vehicle Numbers 2, 5, 10, 14, 18, and 23. The TBI vehicles were Numbers 1, 9, 13, 21, and 24. The new carbureted vehicles were Numbers 3, 7, 11, 15, 17, 19, and 22; and the old carbureted vehicles were Numbers 4, 6, 8, 12, 16, and 20.

Each vehicle was prepared for testing by installing fuel tank drains, fuel tank drain hoses, fuel tank thermocouples, manifold vacuum taps, vacuum lines, and new spark plugs, and cleaning the port fuel injectors by a local contract garage facility and local dealerships. All vehicles passed the tailpipe emissions tests conducted by the State of Colorado Emissions Laboratory. Prior to on-site testing, the engine oil was changed in each vehicle with fresh commercial 5W-30 engine oil. At the completion of the program, the vehicles were returned to the dealer for removal of all test equipment.

No additional mechanical work was performed on the vehicles unless it was necessary for the continuance of the test program. Consequently, all of the vehicles were tested in an "as-received" condition, with no attempt made to correct malfunctioning emission devices or fuel delivery system deficiencies. The results of an on-site inspection of the vehicles are shown in Table II.

IV. TEST FUELS

The test fuels consisted of four fuel types: hydrocarbon-only (Fuels 1-3); hydrocarbon plus 10 vol.% ethanol (Fuels 4-6); hydrocarbon plus 11 vol.% volume methyl tertiary-butyl ether (MTBE) (Fuels 7-9); and hydrocarbon plus ethanol splash blends (Fuels 10-12). With the exception of the splash blends, each of the blends matched the T_{10} and T_{50} distillation temperatures and Reid vapor pressure to the corresponding hydrocarbon-only blend. Splash blends were blends of Fuels 1-3 plus ethanol.

Table III shows test fuel properties averaged across results from the laboratories of four of the participating companies. Samples were obtained from the same drum source on the same date following the conclusion of the low-altitude vehicle testing. Distillation curves for the low, medium, and high volatility fuels are shown in Figures 1, 2, and 3, respectively. Individual laboratory results are shown in Appendix F.

Participating laboratory results surprisingly showed MTBE at about 1% in the "non-MTBE" fuels. No MTBE was intentionally added to these blends. In any case, it has been assumed that these low MTBE levels had no appreciable impact on the overall conclusions.

V. TEST FACILITIES

The high-altitude phase of the program was conducted at the Front Range Airport near Denver, Colorado, at an altitude of 5,486 feet. The test facility was paved, offered access to local roads for vehicle preconditioning, and allowed overnight parking for the test vehicles adjacent to the test course. The test course was laid out on two taxiways, as shown in Figure 4.

The low-altitude phase of the program was conducted at Brainerd International Raceway in Brainerd, Minnesota, at an altitude of 1,226 feet. A schematic of the test site is shown in Figure 5. The facilities included a drive-through fuel/equipment storage and vehicle refueling shed, office space, overnight parking for the test vehicles adjacent to the track, and the track. Drive-ability tests were conducted on the straightaway of the track, with vehicle preconditioning for the next day's testing accomplished by driving four laps around the three-mile track.

Snow removal equipment was available at both locations and used when required.

VI. TEST CONDITIONS

The average run temperatures for the high- and low-altitude phases of the program were 26.7°F and 28.5°F, respectively. Table IV shows average run temperatures for the twelve fuels by the four fuel delivery systems. For the fleet at high altitudes, the matched-volatility 10 vol.% ethanol and the matched-volatility 11 vol.% MTBE fuels had slightly higher run temperatures than the hydrocarbon-only fuel by 6°F and 10°F, respectively. The average run temperature for the splash-blended 10 vol.% ethanol fuels was similar to the hydrocarbon-only fuels (22°F hydrocarbon-only, 24°F splash-blended ethanol). For the fleet at low altitudes, average temperatures for the four fuel compositions were consistent and ranged from 27°F to 31°F.

VII. TEST DESIGN

The statistically designed test program was divided into two phases: a high-altitude phase and a low-altitude phase. The same test vehicles were used for both phases and were divided into three groups: red, blue, and yellow. The assignment of vehicles to each group was approximately equal based upon the various fuel delivery systems. Each rater was assigned the same vehicles for both phases. Raters 1 and 2 were the same individuals for both phases. Rater 3 participated in the high-altitude phase, while Rater 4 participated in the low-altitude phase. Both Raters 3 and 4 were assigned the same vehicles. Each vehicle group was assigned a different fuel for each test day. All fuels

were tested twice in the high-altitude phase. With the exceptions of Fuels 2, 4, and 8, all fuels were tested twice in the low-altitude phase. Time constraints in this phase precluded duplicate testing of all fuels. Details of this test program are given in Appendix C, while fuel/vehicle assignments for each test day are shown in Appendix D. Three vehicles were also tested each day, one vehicle per rater, using the same test fuel (Fuel 3) for determining rater severity levels.

VIII. TEST PROCEDURE

The test procedure for both the high- and low-altitude phases was the CRC Cold-Start and Warmup Driveability Procedure. The driving procedure was preceded by draining the test vehicle's fuel tank, adding the prescribed amount of test fuel, and disconnecting the battery power to the electronic control module for a minimum of one minute to clear any adaptive memory. adaptive memory was reprogrammed to the new fuel using the following driving procedure. All vehicles were "warmed up" by driving fifteen miles using a schedule that included steady states of 25, 35, 45, and 55 miles per hour each for a quarter-mile, and a full stop with a moderate acceleration up to 55 miles per hour. The vehicles were then driven the last two cycles of the Cold-Start and Warmup Driveability Procedure. Driveability malfunctions were recorded for these two cycles and appear as "warm" demerits in Appendix G. These demerits were not used in the computations of this study, but were recorded to assist with the diagnosis of any performance problems with the vehicles. The vehicles were then parked and allowed to soak overnight at ambient temperatures. All vehicles were started the next day using an external battery source in order to eliminate the variability of starting demerits due to a weak battery. After start-up, the vehicles were driven the first six cycles of the Cold-Start and Warmup Driveability Procedure. Driveability malfunctions were recorded for the series of engine idles, accelerations and decelerations, and constant speed cruises; these malfunctions appear as "cold" demerits in Appendix G. Cold-start driveability analysis is based on these six cycles as in previous test programs. A detailed description of the test procedure and rating system is given in Appendix C.

IX. DISCUSSION OF RESULTS

A complete set of overall test data for both the high- and low-altitude phases may be found in Appendix G. This appendix summarizes the data collected from the individual data sheets. The analysis of data performed as described in the following sections used this data base.

A. Simple Total Weighted Demerit Averages

Average cold total weighted demerit (TWD) data for the program are presented in Tables V through IX. In each table, the numbers shown are the averages of TWD values which include the following rater correction factor to account for the difference in severity between Raters 3 and 4:

Rater 3 TWD adjustment = $(\sqrt{TWD} + 1.89)^2$

In all other respects, the averages shown represent the averages of raw TWD values.

Tables V and VI show the average high- and low-altitude results, respectively, for each fuel in each of the four fuel-system categories: old carbureted, new carbureted, TBI, and PFI. Averages are shown for each of the four fuel compositions and for the average of all twelve fuels. It is clear from the grand fuel averages at each test site that the old carbureted vehicles demonstrated four or five times the TWD's associated with any of the other three vehicle classifications. This is true for each fuel composition at either test site.

Table VII shows the differences (Denver minus Brainerd) between Tables V and VI. Values indicate differences due to the two test sites. Positive values would indicate poorer driveability at Denver (high-altitude site). The twelve-fuel averages at the bottom of the table indicate extremely minor differences in three of the four vehicle categories. The difference of 26 TWD's shown for the new carbureted vehicles indicates the possibility that altitude performance was poorer for this group of vehicles. Some of the individual fuel-composition-by-vehicle-group cell averages also indicate differences in performance which could be considered appreciable. In most of these cases, the average differences shown for each of the three fuels do not show a clear effect.

Table VIII and Table IX show the effects of each of the three oxygenate blends for Denver and Brainerd, respectively. Shown are the individual delta values determined by subtracting TWD values of Fuels 1, 2, and 3 (hydrocarbon-only) from the comparable oxygenated fuel. Fositive values indicate that oxygenated fuels had more demerits than the corresponding hydrocarbon-only fuel. In general, the three-fuel average delta for each fuel composition indicates appreciable differences for each of the oxygenates in the old carbureted vehicle classification. Of course, since TWD values were higher with these vehicles, it is reasonable to assume that TWD differences due to oxygenates will be larger in these The Denver assessment of 11 vol.% MTBE in the old carbureted vehicles indicates somewhat lesser degradation in performance (12.1 TWD's) than either the Denver or Brainerd data with the other two oxygenates. The data indicate, however, that the MTBE runs in Denver were conducted at ambient temperatures 10°F higher than the hydrocarbon-only fuel runs. It is believed that this scheduling anomaly accounts for the low-delta TWD value for MTBE in Denver.

A second observation from Tables VIII and IX is that the delta values for the matched-volatility ethanol blends in most cases are appreciable even in the TBI and PFI vehicle categories.

B. DATA TRANSFORMATION

Data were analyzed in terms of the square root of the total weighted demerits (TWD). This will be referred to as SQRTWD. The data were transformed in this way for several reasons:

- The fitting error of the model was normalized across the entire range of TWD values.
- By using square root of TWD, the predicted (fitted) values were positive numbers.

C. ANALYSIS OF VARIANCE

The levels of statistical significance found in this analysis relate to the observations made during the study using trained raters. This program was not designed to correlate customer response with the response of the trained raters.

1. Rater_Correction

The results were analyzed using SAS¹. The specific procedure used for the analysis was the General Linear Model (GLM) procedure. The first analysis done was a correction for the third rater. Vehicles 22, 23, and 24, were run on Fuel 3, and each was rated by all three raters at Denver and at Brainerd; however, only two raters (1 and 2) were common to both sites. Rater 3 was found to produce lower TWD's than raters 1 and 2 at Denver, while Rater 4 was much closer to Raters 1 and 2 at Brainerd. An analysis of variance was performed to find the effect of the different Rater 3 on SQRTWD. The model used to analyze the rater effects utilized run temperature, rater, site, rater-by-site interaction, and vehicle as parameters. This analysis yielded a correction of 1.89 in SQRTWD to be added to Rater 3 at the high-altitude site. All subsequent analysis of the data used this rater correction.

SAS Institute, Inc., "SAS User's Guide: Basics, Version 5 Edition," 1985.

SAS Institute, Inc., "SAS User's Guide: Statistics, Version 5 Edition," 1985.

Rater Correction

	SORTWD	TWD
Rater 1	10.037	100.74
Rater 2	10.550	111.30
Rater 3	7.886	62.19
Rater 3 (corrected)	9.776	95.57
Rater 4	9.777	95.58

2. Full Model Analysis

The inital analysis of variance allowed only for main effects and two-factor interactions. It excluded, however, the error effect terms of the interaction of the vehicle (vehicle group) with the other main variables. This gives overly optimistic significance values, as it uses only the residual error for all the error terms in the analysis. It does, however, find the terms which are not significant so that they can be dropped in a second analysis. The following interactions were found to be not significant:

site * oxygenate
site * volatility
oxygenate * volatility
oxygenate * vehicle group

This means that the differences between oxygenates are not statistically different at Denver and at Brainerd; the volatility effects are not statistically different at Denver than at Brainerd; and in each volatility class, the oxygenate effects are not statistically different.

3. Reduced Model Analysis - Second Pass

The effects which were not found to be statistically significant in the full model were deleted and a second analysis was run. This analysis was designed to test the statistical significance of the interaction of each of the main effects of the model with the vehicle (vehicle group) term. This term is a "nested" term because each vehicle is associated (or nested within) with only one vehicle group. This analysis gave the following observations:

Run temperature (air temperature at start of run) effects:
 Only vehicle group interacts with run temperature; oxygenate and site interaction with run temperature are not significant.

- Site * vehicle group interaction is not significant.
- Volatility * vehicle group interaction is not significant.
- Vehicle group is highly significant.
- Volatility and oxygenate are highly significant effects.
- Significant error terms of the form (X) * vehicle (vehicle group) are:

site * vehicle (vehicle group)
volatility * vehicle (vehicle group)

These results led to the third pass. The third pass model deleted all terms that were not significant except for "site."

4. Reduced Model Analysis - Third Pass

The effects of all significant variables (and site) are discussed in terms of the Least Square Means (LSM) for each factor level. Least Square Means are a method of averaging, performed by the GLM procedure, which averages the effect over all the other test variables in the model. The SAS program, code, and output for this analysis appear in Appendix H.

a) Run Temperature

Although the program was not designed to evaluate test temperature, a significant effect was found. All vehicle groups were responsive to test temperature. The response of SQRTWD to temperature for each of the vehicle groups is shown in the following table:

New PFI	-0.06	SQRTWD/DEG F
New TBI	-0.08	SQRTWD/DEG F
New Carbureted	-0.10	SQRTWD/DEG F
Average New Vehicle	-0.08	SQRTWD/DEG F
Old Carbureted	-0.13	SORTWD/DEG F

The standard error of the pairwise differences is 0.018 SQRTWD/DEG F.

Over the range of 10°F to 40°F , the temperature effect for the pre-1980 vehicles (old carbureted) at 363 average TWD's was a decrease of 4.9 TWD's per degree Fahrenheit increase in ambient temperature. The effect for the new vehicles at an average TWD level of 70 was a decrease of 1.3 TWD's per degree Fahrenheit increase in ambient temperature, which was significantly different from the pre-1980 vehicle effect (p < 0.01).

The effect is calculated by taking the SQRTWD at the average demerit level in question and subtracting the response factor given above from it. This quantity is then squared and subtracted from the square of SQRTWD (the TWD).

In equation form:

Delta TWD/deg F = TWD - $[(SORTWD) - x]^2$

where x = the response factor from the above table

b) Site

The difference in TWD's at high altitude (Denver, 5486 feet) and at low altitude (Brainerd, 1226 feet) was not significant (p = 0.395). The following table shows the results:

SITE	SORTWD	TWD	
Denver	11.54	133	
Brainerd	11.26	127	

The standard error for the difference is 0.33 SQRTWD.

The effect of site, broken up by vehicle group is as follows:

	Denver		Brain	erd
	SORTWD	TWD	SORTWD	TWD
New PFI	6.92	48	7.23	52
New TBI	8.86	78	8.55	73
New Carbureted	10.02	100	8.66	75
Old Carbureted	18.91	358	19.30	372

The difference between the two sites was statistically significant (p < 0.001) only with the new carbureted vehicles.

The three rater vehicles were also evaluated for site effects. The results are as follows:

	Denver		Brainerd	
<u>Vehicle</u>	SORTWD	TWD	SORTWD	TWD
22	15.67	245	11.38	130
23	5.75	33	5.86	34
24	12.29	151	9.78	96

Site was statistically significant (p < 0.001) for Vehicles 22 and 24. The large vehicle-to-vehicle variability found in the program, however, makes any discussion of vehicle or vehicle-group effects inconclusive.

c) Oxygenate

The average TWD's by oxygenate-type were:

OXYGENATE	SORTWD	TWD
Hydrocarbon-Only	10.48	110
11% Matched-Volatility MTBE	11.04	122
10% Matched-Volatility Ethanol	11.71	137
10% Splash-Blended Ethanol	10.84	118

For volatility-matched fuels, average TWD's were: 110 for hydrocarbon-only fuels; 122 for 11 vol.% matched-volatility MTBE fuels; and 137 for 10 vol.% matched-volatility ethanol fuels. Each of these values was significantly different (p < 0.01) from each other.

Average TWD's were 137 for the 10 vol.% matched-volatility ethanol fuels and 118 for the 10 vol.% splash-blended ethanol fuels. This difference was significantly different (p < 0.01).

Average TWD's for the 10 vol.% splash-blended ethanol fuels were 118. The splash-blended ethanol fuels performed significantly poorer (p < 0.01) than the hydrocarbon-only fuels (TWD = 110). Volatility-adjusted MTBE blends were not significantly different from splash-blended ethanol (p = 0.155).

Despite the oxygenate-vehicle group term's not being significant, it is of interest to calculate the oxygenate effect by vehicle group:

NEW CARBURETED

OXYGENATE	SORTWD	TWD
Hydrocarbon-Only	8.78	77
11% Matched-Volatility MTBE	9.32	87
10% Matched-Volatility Ethanol	10.30	106
10% Splash-Blended Ethanol	9.03	81

In the new carbureted group, only the 10 vol.% matched-volatility gasoline-ethanol blend was significantly different from each of the other three fuels.

<u>PFI</u>

OXYGENATE	SORTWD	TWD
Hydrocarbon-Only	6.92	48
11% Matched-Volatility MTBE	7.19	52
10% Matched-Volatility Ethanol	7.53	57
10% Splash-Blended Ethanol	6.63	44

In the PFI group, the 10 vol.% matched-volatility gasoline-ethanol blend was significantly different from the 10 vol.% splash-blended gasoline-ethanol blend. No other combinations were significantly different.

TBI

OXYGENATE	SORTWD	TWD
Hydrocarbon-Only	8.38	70
11% Matched-Volatility MTBE	8.63	74
10% Matched-Volatility Ethanol	9.53	91
10% Splash-Blended Ethanol	8.32	69

In the TBI group, only the 10 vol.% matched-volatility gasoline-ethanol blend was significantly different from the other three fuels.

OLD CARBURETED

OXYGENATE	SORTWD	TWD
Hydrocarbon-only	17.90	320
11% Matched-Volatility MTBE	19.15	367
10% Matched-Volatility Ethanol	19.93	397
10% Splash-Blended Ethanol	19.34	374

In the old carbureted group, the 10 vol.% matched-volatility gasoline-ethanol blend was significantly different from the hydrocarbon-only fuel and the 11 vol.% matched-volatility gasoline-MTBE blend. The hydrocarbon-only fuel was significantly different from all the other fuels.

d) Volatility

The three fuels used in each oxygenate group were divided into three volatility classes. T_{10} values of $110^{\circ}F$ were labeled as low, while T_{10} values of $140^{\circ}F$ were labeled as high. T_{50} values of $200^{\circ}F$ were labeled as low, while T_{50} values of $230^{\circ}F$ were labeled as high. The average SQRTWD and TWD's for the three volatility levels of the test fuels are shown in the following table:

VOL.	<u>ATILITY</u>		SORTWD	TWD
$\underline{\mathbf{T}}_{10}/\underline{\mathbf{T}}_{50}$	<u> T</u> 10	<u> T</u> 50		
Low/Low	110	200	10.24	105
Low/High	110	230	11.19	125
High/High	140	230	12.77	163

All the differences were significant (p < 0.001). The standard error of the pairwise differences was 0.30 units of SQRTWD. As expected, increasing T_{10} and/or T_{50} gave poorer performance. The effects shown above were independent of oxygenate and vehicle group. It is of interest, however, to calculate the above averages by vehicle group:

NEW CARBURETED

	VOLATILIT	<u>¥</u>	SORTWD	TWD
T_{10}/T_{50}	<u>T</u> 10	<u> T</u> 50		
Low/Low	110	200	8.02	64
Low/High	110	230	9.15	84
High/High	140	230	10.82	117

All the above differences were significant in this group.

PFI

	VOLATILITY		SORTWD	TWD
$\underline{\mathbf{T}}_{10}/\underline{\mathbf{T}}_{50}$	<u>T</u> 10	<u>T</u> 50		
Low/Low	110	200	6.42	41
Low/High	110	230	6.74	45
High/High	140	230	7.91	63

For the PFI vehicles, demerit levels with the low/low fuel series and the low/high fuel series were not significantly different. The high/high fuel series was significantly different from the other two fuel series.

TBI

	VOLATILITY		SORTWD	TWD
<u>T</u> 10/T50	<u>T</u> 10	<u> T</u> 50		
Low/Low	110	200	7.45	56
Low/High	110	230	8.38	70
High/High	140	230	10.17	103

All differences for the TBI vehicles were significant.

OLD CARBURETED

	VOLATILITY	<u> </u>	SORTWD	TWD
<u>T</u> 10/T50	<u>T</u> 10	<u> </u>		
Low/Low	110	200	17.30	302
Low/High	110	230	19.15	367
High/High	140	230	20.57	423

All the differences among the three volatility levels were significantly different for the old carbureted vehicles.

e) Vehicle Group

The SQRTWD and TWD's by vehicle group are shown in the following table:

VEHICLE GROUP	SORTWD	TWD
PFI	7.05	50
TBI	8.66	75
NEW CARB	9.30	86
OLD CARB	19.06	363

The standard error of pairwise differences was 1.19 units of SQRTWD. Only the old carbureted vehicles were highly significantly different from all the others (p < 0.0001). The highest significance level between any of the new car types is between new carbureted and PFI at 93 percent (p < 0.07).

D. FUEL DISTILLATION EFFECTS

A regression analysis was performed to evaluate the effects of the fuel parameters which were measured. The actual distillation results were used for the analysis. Two models were constructed. The first used each oxygenate type separately; the second used the oxygen content of the fuel.

Several models were constructed with the T_{30} distillation parameter, all yielding a negative term for T_{30} . This negative term occurs because the effect of the oxygenates is large at T_{30} . The test design did not control the T_{30} of the fuel.

Another caution in interpreting the models presented here is that the T_{10} and T_{50} terms were not fully investigated. The high T_{10} , low T_{50} combination was not tested.

1. T₁₀, T₅₀, and Oxygenate Type Analysis

A linear regression using the SAS GLM procedure on the oxygenate type, T_{10} , and T_{50} data yielded the following equation:

The R^2 for this model is 0.980; the standard error is 0.23.

2. T₁₀, T₅₀, and Percent Oxygen Analysis

An analysis using the SAS GLM procedure on the percent oxygen in the fuel, T_{10} , and T_{50} data yielded the following equation:

SQRTWD = -1.15 +0.31(Mass % Oxygen in Fuel) +0.047 T10 +0.027 T50

The \mathbb{R}^2 for this model is 0.979; the standard error is 0.20.

E. CYCLE ANALYSIS

An investigation was made of the relative contribution of each part of the driving cycle to determine if the test length could be shortened.

The SQRTWD results were sorted into groups by driving cycle. The cycles were defined as the starting procedure, called Cycle 0, and each line of driving maneuvers on the data sheet. This yielded a total of seven cycles. The results were then sorted by vehicle group. The data were then normalized by dividing each group's average SQRTWD in each cycle by that group's total SQRTWD. These results are shown in Figure 6. For all four vehicle groups, the first driving cycle had the highest SQRTWD total. The number of demerits decreased sharply for the TBI and new carbureted vehicles. The old carbureted and PFI vehicles also decreased, but not as rapidly.

An analysis of the SQRTWD results by fuel and driving cycle are shown in Figure 7. The twelve different fuels all follow the same pattern. One fuel, Fuel 10, was slightly higher at Cycle 1 and slightly lower at Cycle 2. Overall, all fuels fall in the same range.

Based on these observations, it appears that it may be possible in the future to delete the last two cycles without loss of discrimination among the various vehicle groups or fuels. Similar analyses by oxygenate type and by volatility level would be required, however, before any conclusions are drawn concerning the number of cycles in the driving procedure.

T A B L E S AND

FIGURES

TABLE I

TEST VEHICLES

1987 Chevrolet Caprice 5.0 1987 Plymouth Horizon 2.2	Carbureted Carbureted Carbureted Carbureted Carbureted
1987 Plymouth Horizon 2.2	Carbureted Carbureted Carbureted
	Carbureted Carbureted
1988 Chrysler Fifth Avenue 5.2	Carbureted
1987 Honda Civic 1.5	
1987 Ford Escort 1.9	carbureced
1987 Nissan Sentra 1.6	Carbureted
1988 Chevrolet Astro 4.3	Throttle-Body-Injected
1987 Mercury Cougar 3.8	Throttle-Body-Injected
1987 Chrysler LeBaron 2.5	Throttle-Body-Injected
1987 Buick Century 2.5	Throttle-Body-Injected
1987 Buick LeSabre 3.8	Port-Fuel-Injected
1987 Ford Aerostar 3.0	Port-Fuel-Injected
1987 Ford LTD Crown Victoria 5.0	Port-Fuel-Injected
1987 Chrysler LeBaron (turbo) 2.2	Port-Fuel-Injected
1987 Toyota Camry (four-valve) 2.0	Port-Fuel-Injected
1978 Dodge Van 5.9	Carbureted
1979 Ford Fairmont 2.3	Carbureted
1979 Plymouth Volare 5.2	Carbureted
1979 Dodge Pickup Truck 5.9	Carbureted
1979 Pontiac LeMans 3.8	Carbureted
1979 Ford Van 5.0	Carbureted
Rater Comparison Vehicles:	
1987 Dodge Charger 2.2 1987 Toyota Camry (four-valve) 2.0 1987 Buick Century 2.5	Carbureted Port-Fuel-Injected Throttle-Body-Injected

TABLE II

VEHICLE MECHANICAL PROBLEMS*

<u>Vehicle</u>	Vehicle Group	Problem	Evaluated Cause
4	Old Carbureted	Acceleration stalls	Tank pickup plugged
6	Old Carbureted	Acceleration stalls	No heated air to carburetor, electric choke modified, and no EGR
8	Old Carbureted	No-starts & acceleration stalls	Choke misadjusted, no heated air to carburetor, and no forward gear when cold
12	Old Carbureted	Down on power - no major problem	Loose timing chain and carburetor misadjusted
15	New Carbureted	Deceleration stalls	Pump cavitation due to slosh on turnaround
16	Old Carbureted	No-starts & acceleration stalls	Choke inoperative, accelerator pump poor, and no heated air to carburetor
20	Old Carbureted	No-starts & acceleration stalls	Choke modified, no heated air to carburetor, and no EGR

^{*} All vehicles listed in this table, except Vehicle 4, were evaluated at the end of the program to determine the probable cause of these chronic problems. With the exception of Vehicle 4, no attempt was made to repair these vehicles, as this would have changed the conditions under which the data were being collected. Vehicle 4, however, was repaired when it became evident that the plugged fuel tank pickup was preventing completion of the runs.

TABLE 111

RESULTS OF ANALYSES FOR THE 1988 CRC DRIVEABILITY PROGRAM FUELS

Sumary

	-	2	က	4	rc	9	7	æ	6	10	11	12
RVP, psi	13.4	13.6	8.6	13.7	13.3	9.5	13.8	13.4	9.5	13.9	13.5	10.6
Dist, % Evap., °F												
IBP 5 vol.% 10 vol.% 20 vol.% 40 vol.% 50 vol.% 70 vol.% 80 vol.% 95 vol.% 95 vol.% FP vol.% 95 vol.% 95 vol.% 87 vol.% 98 vol.% 89 vol.% 80 vol.% 98 vol.% 80	99 109 1128 173 200 230 230 269 311 33 34 114	79 108 1134 163 198 234 289 333 346 383 45 45	120 120 138 177 222 235 235 342 342 333 33 64	83 111 111 128 142 204 204 330 343 362 37 382 382 397 30 30 68	84 106 1114 1133 147 277 277 302 335 346 381 116	101 129 142 172 172 238 250 250 332 346 386 386 60	80 100 106 126 147 173 203 203 342 342 342 342 342 344 346 347 347 347 347 348 348 348 348 348 348 348 348 348 348	99 107 132 132 158 228 228 277 302 329 344 385 33 33	21 141 173 173 198 217 234 248 301 332 349 377 38 38	253 32 32 32 32 36 336 348 388 388 388 36 36 37 37	84 106 112 130 143 156 193 273 301 344 391 116 40	120 133 148 168 168 178 183 183 134 134 134 134 63
Oxygenate Content, % Ethanol MTBE	<0.1 1.0	<0.1 1.0	<0.1 1.4	9.3	8.8 0.8	9.4	<0.1 11.4	<0.1 10.4	<0.1 11.3	7.9	9.8	9.9

TABLE IV

AVERAGE RUN TEMPERATURES (Degrees Fahrenheit)

	Hydr	Hydrocarbon-onl	yluo 3	Hydrocarbon + Ethano (Matched-Vola	- ~	10 vol.% tility)	Hydroca (Match	Hydrocarbon + 11 vol.% MTBE (Matched-Volatility)	1 vol.%	Hydroca (Sp1	Hydrocarbon + 10 vol.% Ethanol (Splash-Blended)	0 vol.%
	•	4	·†	-	·	,	-		,	:	;	
					H	High-Altitude	de Phase					
Fuel System												
01d Carbureted New Carbureted TBI PFI	26 25 26 27	18 20 17 18	23 23 23 23	333	20 20 21	3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	32 32 32 33	33 33 34 34	32 33 30	18 21 19 18	22 23 23	32 32 32 32
Average	56	18	23	31	20	34	32	32	31	19	22	32
Average by fuel composition		22			88			32			24	
					Low	Low-Altitude	e Phase					
Fuel System												
01d Carbureted New Carbureted TBI PFI	32 32 33	25 23 28 28	26 24 24	30 34 27	26 25 27 23	28 30 27 27	28 29 28 28	29 32 31	23 23 23	32 36 36 36	28 30 23 23	31 32 30 31
Average	32	56	56	30	52	78	28	30	23	35	28	31
Average by fuel composition		58			58			27			31	

TABLE V

AVERAGE TOTAL WEIGHTED DEMERITS (RATER-ADJUSTED)

High-Altitude Phase (Denver)

		Fuel-System T	уре	
Fuel	01d	New		
Number	<u>Carbureted</u>	<u>Carbureted</u>	TBI	PFI
Hydrocarbon-Only				
1	263.4	74.1	60.2	39.4
2	385.4	115.3	80.7	73.1
3	403.3	127.4	98.1	67.2
Average	350.7	105.6	79.6	59.9
Matched-Volatility Ethanol				
4	305.7	95.0	67.4	37.5
5	439.6	127.6	106.0	68.6
6	441.0	154.6	118.4	57.6
Average	395.4	125.7	97.2	54.6
Matched-Volatility MTBE				
7	279.0	84.9	55.9	40.8
8	333.5	92.8	69.2	50.3
9	403.4	114.2	106.6	79.5
Average	338.6	97.3	77.2	56.9
Splash-Blended Ethanol				
10	370.2	69.3	64.8	43.3
11	405.0	97.0	78.6	42.1
12	392.7	132.9	96.5	67.4
Average	389.3	99.7	80.0	50.9
Grand Average	368.5	107.1	83.5	55.6

TABLE VI

AVERAGE TOTAL WEIGHTED DEMERITS (RATER-ADJUSTED)

Low-Altitude Phase (Brainerd)

	Fuel-System Type			
Fuel	01d	New		
Number	<u>Carbureted</u>	<u>Carbureted</u>	TBI	PFI
Hydrocarbon-Only				
1	263.7	46.0	49.0	60.5
2	341.0	92.0	68.4	41.0
3	385.0	87.9	104.7	61.3
Average	329.9	75.4	74.0	54.4
Matched-Volatility Ethanol				
4	364.5	62.6	58.8	92.8
5	376.1	85.3	72.8	60.7
6	463.5	120.1	133.6	81.4
Average	401.3	89.3	88.4	78.3
Matched-Volatility MTBE				
7	341.3	52.5	57.7	45.0
8	386.3	74.4	58.4	48.4
9	446.9	113.4	99.4	68.0
				
Average	392.4	80.1	71.8	53.6
Splash-Blended Ethanol				
10	253.1	49.1	46.7	39.4
11	394.3	78.7	67.9	46.4
12	442.7	104.6	86.1	56.1
Average	363.4	77.4	66.9	47.3
Grand Average	371.8	80.6	75.3	58.4

TABLE VII

EFFECT OF ALTITUDE ON RATER-ADJUSTED TOTAL WEIGHTED DEMERITS

(Denver Minus Brainerd)

	Fuel-System Type			
.Fue1	01d	New		
Number	<u>Carbureted</u>	<u>Carbureted</u>	TBI	<u>PFI</u>
Hydrocarbon-Only				
1	-0.3	28.1	11.2	-21.1
2 3	44.4	23.1	12.3	32.1
3	18.2	39.5	-6.6	5.9
Average	20.8	30.2	5.6	5.5
Matched-Volatility Ethanol				
4	-58.8	32.4	8.6	-55.3
5	63.5	42.3	33.2	7.9
6	-22.5	34.5	-15.2	-23.8
Average	- 5.9	36.4	8.8	-23.7
Matched-Volatility MTBE				
7	-62.3	32.4	-1.8	-4.2
8	-52.8	18.4	1.9	10.8
9	-43.5	0.8	7.2	11.5
				
Average	-53.8	17.2	5.4	3.3
Splash-Blended Ethanol				
10	117.1	20.2	18.1	3.9
11	10.7	18.3	10.7	-4.3
12	-50.0	28.3	10.4	11.3
Average	25.9	22.3	13.1	3.6
Grand Average	- 2.0	26.5	8.2	-2.8

TABLE VIII

EFFECT OF OXYGENATES ON RATER-ADJUSTED TOTAL WEIGHTED DEMERITS

High-Altitude Phase (Denver)

	Fuel-System Type			
Fuel	01d	New	TOT	DET
ruei	Carbureted	<u>Carbureted</u>	<u>TBI</u>	<u>PFI</u>
Effect of 10% Matched- Volatility Ethanol				
4 - 1	42.3	20.9	7.2	-1.9
5 - 2	54.2	12.3	25.3	-4.5
6 - 3	37.7	27.2	20.3	-9.6
Average	44.7	20.1	17.6	-5.3
Effect of 11% Matched- Volatility MTBE				
7 - 1	15.6	10.8	4.3	1.4
8 - 2 9 - 3	-51.9 0.1	-22.5 -13.2	-11.5 8.5	-22.8 12.3
9 - 3	····	-13.2	0.5	12.5
Average	12.1	-8.3	-2.4	-3.0
Effect of 10% Splash- Blended Ethanol				
10 - 1	106.8	-4.8	4.6	3.9
11 - 2	19.6	-18.3	-2.1	-3.1
12 - 3	-10.6	5.5	-1.6	0.2
Average	38.7	-5.9	0.4	-9.0

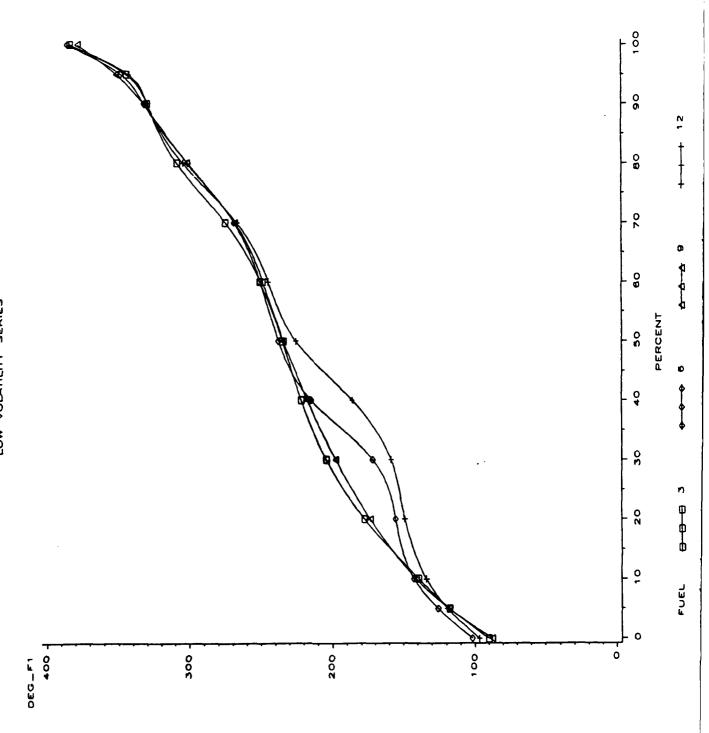
TABLE IX

EFFECT OF OXYGENATES ON RATER-ADJUSTED TOTAL WEIGHTED DEMERITS

Low-Altitude Phase (Brainerd)

	Fuel-System Type			
Fue1	01d <u>Carbureted</u>	New <u>Carbureted</u>	TBI	PFI
Effect of 10% Matched- Volatility Et!.anol				
4 - 1 5 - 2	100.8 35.1	16.6 -6.9	9.8 4.4	32.3 19.7
6 - 3	78.5	32.2	28.9	20.1
Average	71.4	13.9	14.4	33.9
Effect of 11% Matched- Volatility MTBE				
7 - 1 8 - 2	77.6 45.3	6.5 -17.8	8.7 -10.0	-15.5 7.4
9 - 3	61.9	25.5	-5.3	6.7
Average	57.4	4.7	-2.2	-0.8
Effect of 10% Splash- Blended Ethanol				
10 - 1 11 - 2	-10.6 53.3	3.1 -13.5	-2.3 -0.5	-21.1 5.4
12 - 3	57.7	16.7	-18.6	-5.2
Average	33.5	2.0	-7.1	-7.1

FIGURE 1



FUEL DISTILLATION

FIGURE 2

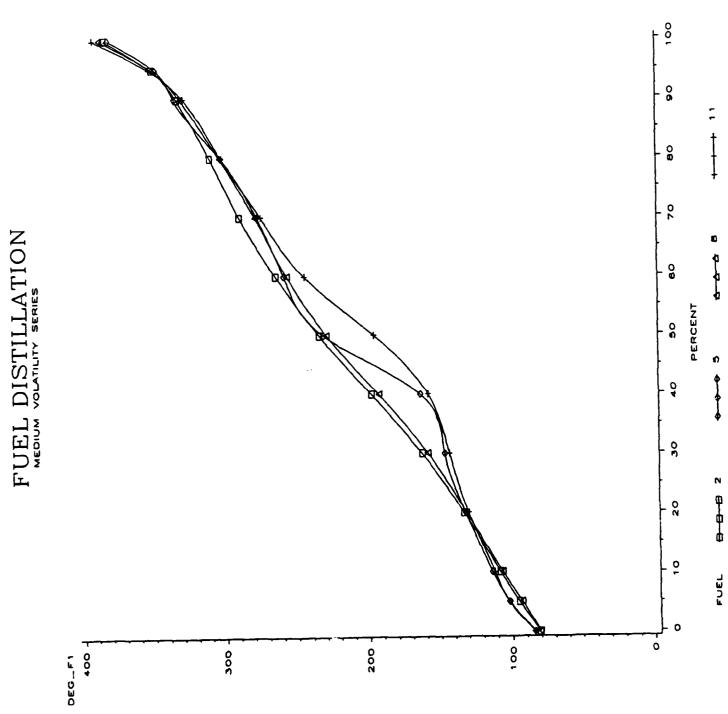
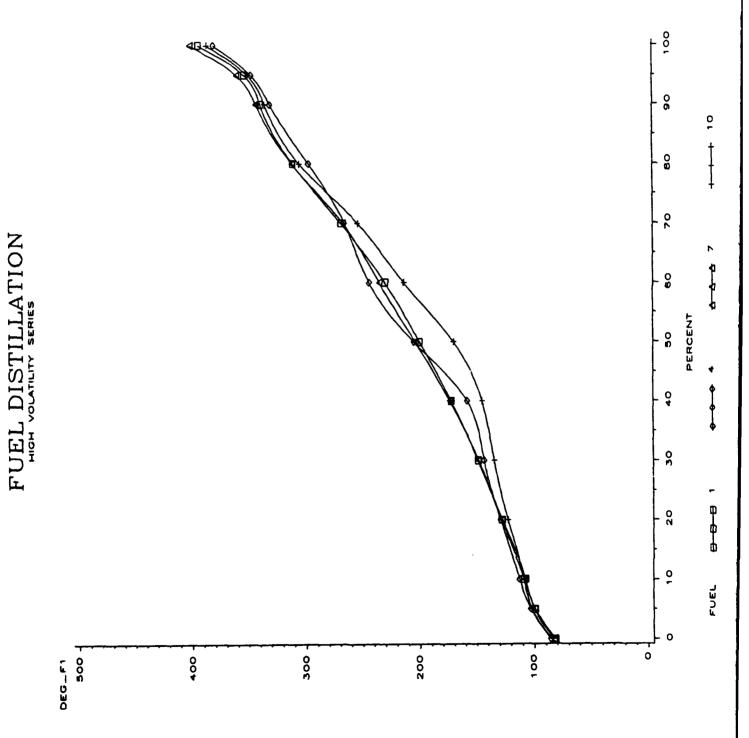
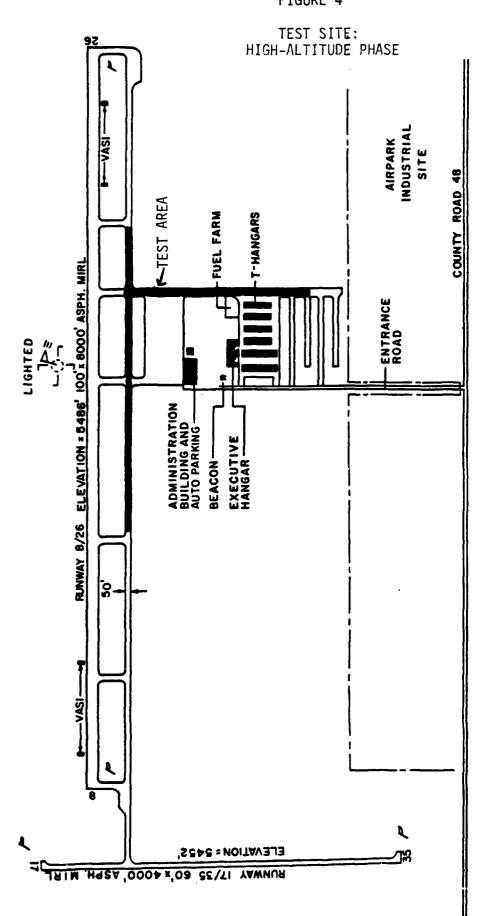


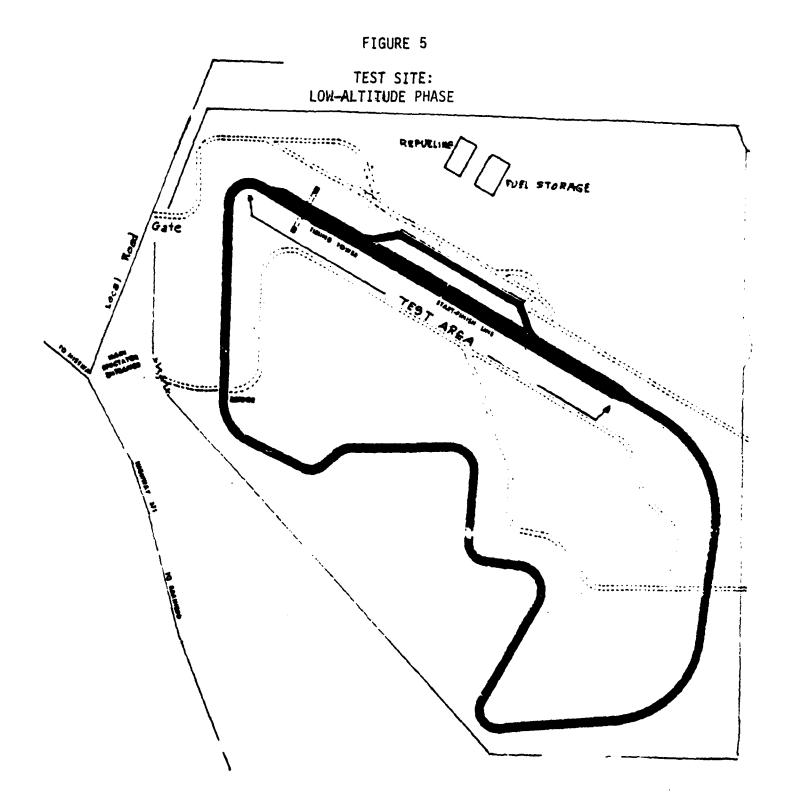
FIGURE 3





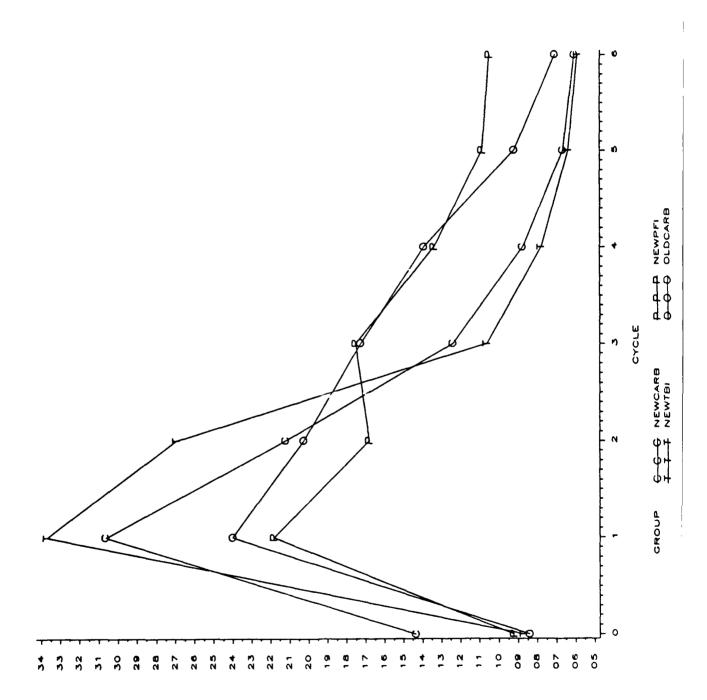
FRONT RANGE AIRPORT

(Denver, Colorado)



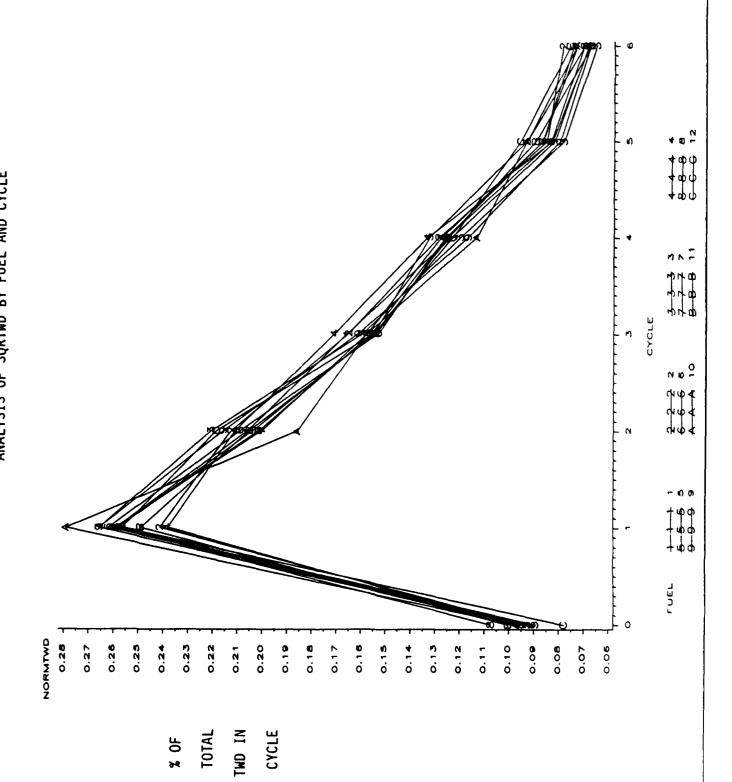
BRAINERD INTERNATIONAL RACEWAY

FIGURE 6
DISTRIBUTION OF TWD BY CYCLE



% OF TOTAL TWD IN CYCLE

FIGURE 7
ANALYSIS OF SQRTWD BY FUEL AND CYCLE



APPENDIX A

MEMBERSHIP
OF THE
1988 CRC DRIVEABILITY ANALYSIS PANEL

MEMBERSHIP OF THE

1988 CRC DRIVEABILITY ANALYSIS PANEL

NAME	AFFILIATION
P. A. Yaccarino, Leader	General Motors Research Laboratories
D. A. Barker	Shell Development Company
J. H. Baudino	AutoResearch Laboratories, Inc.
J. P. Graham	Chevron Research Company
L. J. Painter	Consultant
R. M. Reuter	Texaco Inc.
E. H. Schanerberger E. D. Steinke	Ford Motor Company Sun Refining & Marketing Company
J. H. Steury L. J. Sumansky C. T. Valade	Amoco Oil Company Mobil Research & Development Corporation Chrysler Corporation

APPENDIX B

PARTICIPANTS IN THE 1988 CRC DRIVEABILITY PROGRAM

PARTICIPANTS IN THE 1988 CRC VOLATILITY PROGRAM ON THE EFFECT OF OXYGENATED FUELS AND

ALTITUDE ON DRIVEABILITY AT LOW AMBIENT TEMPERATURES

Name	Company	Participation: High-Altitude Phase	Participation: Low-Altitude Phase
Bill Allen	Volvo of North America	X	
Dave Barker	Shell Development Company	X	X
Jack Baudino	AutoResearch Labs, Inc.	X	
Don Burnett	Phillips 66 Company		X
Ed Carhart	Texaco Inc.	χ	X
John Deffner	Chevron Research Company	X	
Jimmy Douglass	Shell Development Company		X
Dave Essmann	Consultant		X
Beth Evans	Coordinating Res. Council		X
Art Feyers	Chrysler Corporation	X	
John Graham	Chevron Research Company	X	X
Keith Houser	Chevron Research Company	X	
Scott Jorgensen	GM Research Laboratories	X	X
Toshio Kobayashi	Nissan Research & Develop.	X	
Doug McCorkell	Unocal Corporation	X	
Sterling McFee	Marathon Petroleum Co.	X	
Jim Macias	Shell Development Company	X	
Dick Nelson	Consultant		X
Francis O'Neill	Colorado Dept. of Health	X	
Dennis Poma	Amoco Oil Company		X
Doug Rathe	Shell Development Company	X	
Dick Robison	Colorado Dept. of Health	X	
E. H. Schanerberger	Ford Motor Company	X	X
Lieu Steinke	Sun Refining & Marketing	X	
John Steury	Amoco Oil Company	X	
Linda Sumansky	Mobil Research & Develop.	X	
Dave Swiderski	Chrysler Corporation		X
Vince Thomas	Amoco Oil Company		X
Chuck Valade	Chrysler Corporation	χ	X
Greg Van Meveren	AutoResearch Labs, Inc.		X
Phil Yaccarino	GM Research Laboratories	X	X

APPENDIX C

1988 CRC VOLATILITY PROGRAM ON THE EFFECT OF OXYGENATED FUELS AND ALTITUDE ON DRIVEABILITY AT LOW AMBIENT TEMPERATURES

COORDINATING RESEARCH COUNCIL

INCORPORATED

219 PERIMETER CENTER PARKWAY ATLANTA, GEORGIA 30346 (404) 396-3400

Not to be Published

1988 CRC VOLATILITY PROGRAM

ON THE

EFFECT OF OXYGENATED FUELS AND ALTITUDE ON DRIVEABILITY AT LOW AMBIENT TEMPERATURES

(CRC Project No. CM-118-88)

Prepared by the CRC-Automotive Volatility Group

November 1987

CRC-AUTOMOTIVE 1988 VOLATILITY PROGRAM

ON DRIVEABILITY AT LOW AMBIENT TEMPERATURES

Objective

The objective of the 1988 CRC Volatility Group program is to determine the effects of altitude and fuel oxygenates at low ambient temperatures upon trained-rater cold-start driveability of closed- and open-loop vehicles. The program will compare the relationship, at altitude, between driveability and the 10 and 50 percent distillation temperatures for hydrocarbon-only and hydrocarbon/oxygenate (ethanol and MTBE) blends.

Introduction

There has been much discussion and proposed legislation in many states concerning the use of oxygenated fuels to reduce ambient CO levels. Several metropolitan areas are in the process of requiring the use of oxygenated fuels during the winter months. Denver, Colorado, is at the forefront of this movement. They are planning a phase-in of their program over several years and are inviting comment on any problems which may be associated with the proposal. The Denver area has a high percentage of vehicles which are open-loop-controlled. Based upon past experience, these open-loop vehicles should have the greatest reduction of CO with the use of oxygenated fuels in high-altitude areas.

The CRC Volatility Group has run several programs in recent years to investigate the effect of oxygenated fuels on driveability. Most of the recent Volatility Group work has concentrated on closed-loop, fuel-injected vehicles. There is no recent information, however, on the effects of oxygenated blends at altitude.

Test Temperatures

The test temperature will be targeted for 15-40°F. This is the range of temperature found in Denver during the winter (January) when the use of oxygenated fuels will be required.

Test Fuels

The test fuels will consist of four fuel compositions [hydrocarbon-only, hydrocarbon + 10 vol% ethanol (volatility-matched), hydrocarbon + 10 vol% ethanol (splash-blended), and hydrocarbon + 11 vol% methyl-tertiary-butyl-ether (MTBE, volatility-matched)]. The fuels provide independent variation in two volatility parameters: 10% and 50% distillation temperatures. The term "volatility-matched" refers to the 10% and 50% distillation temperatures.

The fuel set design would require twelve fuels (three for each of the four fuel compositions). The specifications for the test fuels are shown in Table C-I.

The fuel supplier will provide the following inspections:

Rvp, psi (Dry Method, Modification of D 323)
Distillation (D 86)
API Gravity (D 287)
T_{V/L=20} (Hg Modification of D 2533)
FIA (Hydrocarbon-Only Fuels)
Benzene, vol% (GC)
Alcohol Content, vol% (GC)
Calculated Latent Heat of Vaporization
Net Heating Value (Modified D 240)
H/C Ratio (Combustion Method)

Test Vehicles

Tests will be conducted with fifteen 1988 model-year cars and light trucks. These vehicles will all have closed-loop (feedback) fuel-metering systems. Five vehicles will have throttle-body fuel-injection (TBI), five will have port-fuel-injection (PFI), and five will be carburetted. Five open-loop vehicles (drawn from late-model trucks and pre-1980 vehicles) will also be tested. All vehicles will have automatic transmissions. The proposed vehicle list is shown in Table C-II.

Vehicle preparation will include:

- 1) Thorough mechanical inspection.
- Verification of the proper operation of all emissioncontrol and driveability-related devices. This should include a check of idle tailpipe emissions and a check of trouble codes in computer-equipped vehicles. Choke settings of carburetted vehicles will be measured and set to specification.

- 3) Replacement of PFI injectors. If this is not possible, some verification of proper injector flow will be required (i.e., pressure-drop test).
- 4) Installation of manifold vacuum tap.
- 5) Installation of thermocouple in the fuel tank.
- 6) Installation of fuel tank drain.
- 7) Installation of device to cut off power to the electronic control module (ECM). This may be a switch in the electrical feed to the ECM.

Before the testing begins, each vehicle should be run through the driveability procedure with a fuel known to produce few demerits to insure proper vehicle operation.

Test Procedure

The basic test procedure will be the CRC Cold Start and Warmup Driveability Procedure as previously run in 1986/1987.

Many of the closed-loop-controlled vehicles have the ability to update their cold-start and open-loop calibration by using information "learned" during closed-loop operation. This is called adaptive learning. To ensure that all vehicles have adapted to the test fuel, the following procedure modifications will be made:

- Immediately after refueling, disconnect battery power to the ECM for one minute. This will clear any adaptive memory.
- During the fifteen-mile warmup, run the vehicle through a variety of driving conditions (i.e., do not run a constant speed).

Cold start driveability analysis will be based on the initial six cycles as in the previous test programs. The last two cycles will be analyzed separately to indicate warmed-up driveability malfunctions. The test procedure and rating system are included as Attachment A.

Program Duration and Manpower Requirement

Each phase of the program (altitude and sea level) will run for four and one-half weeks. Nine participants are required to be on-site at all times. It is desirable for continuity that raters participate for the full program time of four and one-half weeks.

Test Location and Timing

The high-altitude portion of the program will be conducted from January 11, 1988, through February 10, 1988, at the Front Range Airport, Watkins, Colorado (just outside of Denver). The facility is paved and will offer access to a local highway for vehicle preparation. Snow-removal will be provided by the airport.

The low-altitude portion of the program will be conducted from February 29, 1988, through March 30, 1988, at Brainerd International Raceway, Brainerd, Minnesota. To provide an ice-free and dry surface, salting and sanding of the track will be allowed. Offices and indoor shop areas are also available for our use.

Test Design

There are a total of twenty-seven days (including Saturdays) available for on-site testing for each phase. It should be noted that an "off" day is not really "off," because the vehicle must be prepared for the following day. If all possible days are included, there are thirty-one days available.

A minimum of three days will be needed for setup, rater training, and cleanup.

The test plan will be broken down into two phases:

- I. Twelve test days, all vehicles, Fuels 1-12.
- II. Beginning with the thirteenth day, repeat all vehicles, all fuels except Fuels 1, 4, 7, and 10.

The first twelve days will randomize the order of fuel testing. The vehicle fleet will be broken up into three groups: A, B, and C. The groups will have a mixture of all fuel system types. Raters will be permanently assigned to a vehicle. The test order will be as follows:

	DAY	GROUP A	GROUP B	GROUP C
PHASE I				
	1	1	5	9
	2	10	2	6
	3	7	11	3
	4	4	8	12
	5	11	1	4
	6	8	10	1
	7	2	4	7
	8	12	3	5
	ŏ	6	7	2
	10	9	12	10
	10	9		
	11	5	6	8
	12	3	9	11

Beginning with the thirteenth day, all vehicles will be tested on the same fuel, in case testing has to be truncated due to weather. Fuels will be selected on a random basis, excluding Fuels 1, 4, 7, and 10, which will not be repeated unless time allows.

TABLE C-I TEST FUEL DESIGN LEVELS

<u>Fuel</u>	10% Dist.	50% Dist.
	HYDROCARBON-ONLY	
1 2 3	110 110 140	200 230 230
HYDROCARI	BON + 10 VOL.% ETHANOL (Volatil	ity-Matched)
4 5 6	110 110 140	200 230 230
HYDROCA	ARBON + 11 VOL.% MTBE (Volatili	ty-Matched)
7 8 9	110 110 140	200 230 230
HYDI	ROCARBON + 10 VOL.% ETHANOL (Sp	lashed)
10	Fuel 1 with 10% Ethanol	
11	Fuel 2 with 10% Ethanol	
12	Fuel 3 with 10% Ethanol	

Fuels 1 through 9 shall have a 330°F 90% distillation temperature. Tolerances shall be +5°F on distillation temperatures.

- Minimum delta T_{10} and T_{50} values are also specified as follows:

 a) T_{10} for Fuel 3 shall be at least 25°F higher than Fuels 1 and 2.
 b) T_{10} for Fuel 6 shall be at least 25°F higher than Fuels 4 and 5.
 c) T_{10} for Fuel 9 shall be at least 25°F higher than Fuels 7 and 8.

 - T_{50} for Fuels 2 and 3 shall be at least 25°F higher than Fuel 1.
- T_{50} for Fuels 5 and 6 shall be at least 25°F higher than Fuel 4. f) T_{50} for Fuels 8 and 9 shall be at least 25°F higher than Fuel 7. RVP ranges for all fuels are specified below:

Fuel RVP, psi
$$13.5 \pm 0.5$$
 13.5 ± 0.5 Maximum possible with T_{10} @ 140°F

All fuels shall be unleaded and have a minimum (R+M)/2 octane rating of 88. fuels shall exhibit no phase separation at 0°F.

Fuels shall contain no more than 3% Benzene.

Fuels shall not exceed the ASTM maximum endpoint specification of 437°F.

Fuels shall not contain more than 40% aromatic.

Fuels shall contain an antioxidant and a corrosion inhibitor.

Ethanol shall be denatured with unleaded gasoline (CDA Formula #20).

TABLE C-II

TEST VEHICLES

Manufacturer	Displacement	Fuel System
General Motors	2.5 Liter	TBI
General Motors	4.3 Liter	TBI
Ford	3.8 Liter	TBI
Chrysler	2.5 Liter	TBI
AMC	1.7 Liter	TBI
General Motors Ford Ford Chrysler (Turbo) Toyota	3.8 Liter 3.0 Liter 5.0 Liter 2.2 Liter 2.0 Liter	PFI PFI PFI PFI PFI
General Motors	5.0 Liter	CARB
Chrysler	2.2 Liter	CARB
Chrysler	5.2 Liter	CARB
Honda	1.5 Liter	CARB
Nissan	1.6 Liter	CARB

Two light-duty trucks and three passenger cars with carburetted, open-loop fuel systems will be used.

ATTACHMENT A

CRC COLD START AND WARMUP DRIVEABILITY PROCEDURE

TEST PROCEDURE AND DATA RECORDING

- A. Record all necessary test information at the top of the data sheet.
- B. Start engine per Owner's Manual Procedure. Record start time.
- C. If engine fails to start after 15 seconds of cranking, stop cranking. Follow Owner's Manual procedure for this situation. Begin cranking and record total cranking time until engine starts.
- D. Record idle quality in "Neutral" or "Park" immediately after start; foot should be removed from accelerator pedal.
- E. If engine stalls, repeat Steps B and C. Record number of stalls and starting time of required restarts.
- F. Allow engine to idle 15 seconds. Apply brakes (right foot), shift to normal drive range, and record idle quality. If engine stalls, restart immediately. Do not record restart time. Record number of stalls. Idle 5 seconds in "Drive".

This completes the start-up portion of the procedure. Note that space on the data sheet has only been provided for two restart times at any idle condition. If three stalls occur at any condition, record the three stalls, restart (without recording time) and proceed to the next scheduled condition.

G. After 5 seconds in "Drive" (Step F), make a light throttle (Lt. th) acceleration from 0-25 mph at constant throttle opening beginning at the predetermined manifold vacuum.* Cruise at 25 mph. At the 0.2 mile marker open throttle to the detent position and accelerate from 25 to 35 mph at constant throttle in high gear. Decelerate to a stop, and at the 0.3 mile marker make a WOT acceleration from 0 to 35 mph. Decelerate to 10 mph and at mile marker 0.4 accelerate at light throttle from 10 to 25 mph. Definitions of light throttle, detent, and WOT accelerations are attached.

^{*} Marked on vacuum gauge.

- H. During the above maneuvers, observe and record the severity of any of the following malfunctions (see attached definitions):
 - 1. Hesitation
 - 2. Stumble
 - 3. Surge
 - 4. Stall
 - 5. Backfire

Record maneuvering stalls on the data sheet in the appropriate column: accelerating or decelerating.

- I. At the 0.5 mile marker, brake moderately to a stop on the right side of the roadway. Idle for 30 seconds in Drive. Record idle quality and number of stalls.
- J. Perform Steps G, H, and I three times (1.5 miles). The mile marker for the beginning of each maneuver is indicated on the data sheet.
- K. At mile marker 1.5, after completing the 30-second idle, make a crowd acceleration (constant predetermined vacuum) from 0-45 mph. Four tenths of a mile is provided for this maneuver. Decelerate from 45 to 25 mph at the 1.9 mile marker, and open throttle to detent position and accelerate from 25 to 35 mph. At 2.0 miles decelerate to a stop and accelerate from 0 to 35 mph at WOT. At 2.1 miles decelerate to 10 mph and accelerate from 10 to 25 mph at light throttle. Rate and record malfunctions in these maneuvers as in Step H. Idle 30 seconds in Drive as in Step I.
- L. Perform Step K one time. Appropriate mile markers for the start of each maneuver are shown on the data sheet.

DEFINITIONS AND EXPLANATIONS

Test Run

Operation of a car throughout the prescribed sequence of operating conditions and/or maneuvers for a single test fuel.

Maneuver

A specified single vehicle operation or change of operating conditions (such as idle, acceleration or cruise) that constitutes one segment of the driveability driving schedule.

Cruise

Operation at a prescribed constant vehicle speed with a fixed throttle position on a level road.

Wide Open Throttle (WOT) Acceleration

"Floorboard" acceleration through the gears from prescribed starting speed. Rate at which throttle is depressed is to be as fast as possible without producing tire squeal or appreciable slippage.

Part-Throttle (PT) Acceleration

An acceleration made an any defined throttle position, or consistent change in throttle position, less than WOT. Several PT accelerations are used. They are:

- 1. Light Throttle (Lt. Th) All light throttle accelerations are begun by opening the throttle to an initial manifold vacuum and maintaining constant throttle position throughout the remainder of the acceleration. The vacuum selected is one inch Hg greater than the initial power cut-in vacuum obtained from carburetor flow curves. However, if a 0-25 mph light throttle maneuver (car warmed up) cannot be completed in 0.1 mile, vacuum is decreased in steps of one inch Hg until the 0-25 maneuver can be completed in 0.1 mile. The selected vacuum is posted in each car.
- 2. Crowd An acceleration made at a constant intake manifold vacuum. To maintain constant vacuum, the throttle opening must be continually increased with increasing engine speed. Crowd accelerations are performed at the same vacuum prescribed for the light throttle acceleration.
- 3. Detent All detent accelerations are begun by opening the throttle to the downshift position as indicated by transmission shift characteristic curves. Manifold vacuum corresponding to this point at 25 mph is posted in each car. Constant throttle position is maintained to 35 mph in this maneuver.

Malfunctions

1. Stall

Any occasion during a test when the engine stops with the ignition on. Three types of stall, indicated by location on the data sheet, are:

- a. Stall; idle Any stall experienced when the vehicle is not in motion, or when a maneuver is not being attempted.
- b. <u>Stall; maneuvering</u> Any stall which occurs during a prescribed maneuver or attempt to maneuver.
- c. <u>Stall; decelerating</u> Any stall which occurs while decelerating between maneuvers.

2. <u>Idle Roughness</u>

An evaluation of the idle quality or degree of smoothness while the engine is idling.

3. Backfire

An explosion in the induction or exhaust system.

4. Hesitation

A temporary lack of vehicle response to opening of the throttle.

5. Stumble

A short, sharp reduction in acceleration after the vehicle is in motion.

6. Surge

Cyclic power fluctuations occurring during acceleration or cruise.

Malfunction Severity Ratings

The number of stalls encountered during any maneuver are to be listed in the appropriate data sheet column. Each of the other malfunctions must be rated by severity and the letter designation entered on the data sheet. The following definitions of severity are to be applied in making such ratings.

- 1. Trace (T) A level of malfunction severity that is just discernible to a test driver but not to most laymen.
- 2. <u>Moderate (M)</u> A level of malfunction severity that is probably noticeable to the average layman.
- 3. Heavy (H) A level of malfunction severity that is pronounced and obvious to both test driver and layman.

Enter a T, M, or H in the appropriate data block to indicate both the occurrence of the malfunction and its severity. More than one type of malfunction may be recorded on each line. If no malfunctions occur, enter a dash (-) to indicate that the maneuver was performed and operation was satisfactory during that maneuver.

DEMERIT CALCULATION SYSTEM

A numerical value for driveability during the CRC test is obtained by assigning demerits to operating malfunctions as shown on Page C-19. Depending upon the type of malfunction, demerits are assigned in various ways. Demerits for poor starting are obtained by subtracting two seconds from the measured starting time. The number of stalls which occur during idle as well as during driving maneuvers are counted separately and assigned demerits as shown on Page C-19. The multiplying x factors of 8 and 32 for idle and maneuvering stalls, respectively, account for the fact that stalls are very undesirable, especially during car maneuvers.

Other malfunctions, such as hesitation, stumble, surge, idle roughness, and backfire, are rated subjectively by the driver on a scale of trace, moderate, or heavy. For these malfunctions, a certain number of demerits is assigned to each of the subjective ratings, However, since all malfunctions are not of equal importance, the demerits are multiplied by the weighting factors shown on Page C-19 to yield weighted demerits.

Finally, weighted demerits, demerits for stalls, and demerits for poor starting are summed to obtain total weighted demerits (TWD), which are used as an indication of driveability during the test. As driveability deteriorates, TWD increases.

A restriction is applied in the totaling of demerits to insure that a stall results in the highest possible number of demerits within a given maneuver. When more than one malfunction occurs during a maneuver, demerits are counted for only the malfunction which had the largest number of weighted demerits. Another restriction is that for each idle period, no more than 3 idle stalls are counted.

METHOD FOR CALCULATING TOTAL WEIGHTED DEMERITS (TWD)

Demerits for Poor Starting:

Demerits = Starting Time(s) - 2

Demerits for Stalls:

Demerits = (No. of Idle Stalls) x 8 + (No. of Maneuvering or Decelerating Stalls) x 32

Demerits for Malfunctions Rated Subjectively:

Demerits for Subjective Ratings

Trace = 1

Moderate = 2

Heavy = 4

Weighting Factors for Each Malfunction

Idle Roughness = 1

Surge = 4

Backfire, Stumble, Hesitation = 6

Weighted Demerits = Demerits x Weighting Factor

Calculation:

Total Weighted Demerits = Weighted Demerits + Demerits for Stalls + Demerits for Poor Starting

NOTE: When more than one malfunction occurs in a driving maneuver, only the malfunction giving the highest weighted demerits is counted.

CRC Driveability Data Sheet

Soak Run Fuel tank X1 X2	Stalls Stalls Stalls Stalls Stalls 1.0 1.0 1.4 1.5 Ruf. stalls Fuel tank X1 X2 1.0 1.1 1.4 1.5 Ruf. stalls Fuel tank X1 X2 1.0 1.0 1.1 1.5 Ruf. stalls Fuel tank X1 X2	2.9 3.6 4.3 4.3
Idle Dr.	0.3 0-35 WOT Staffs 1.3 1.3 Ac Staffs Ac Staffs Ac Staffs Ac Staffs	2.8
Fuel Rater Date	0.2 25.35 Detent Sum: Stalls S	3.4
Car Time, sec.	1.9 25-35 Detent 1.9 25-35 Detent 25 Cruise 1.9 25-35 Detent 25-35 Detent 25 公司 1.9 25	3.3
Starting Starting	0.0 0-25 Lt. Th. Stalls Stalls Stalls Stalls Stalls Stalls Stalls Stalls Stalls	2.2 2.9 3.6 4.3

APPENDIX D

TEST SCHEDULE

TEST SCHEDULE - DENVER

The test plan will be broken down into three phases:

- I. 12 test days, all vehicles, all 12 fuels
- II. 9 test days, all vehicles, a repeat of fuels 2,3,5,6,8,9,11,12
- III. 3 test days, all vehicles, a repeat of fuels 1,4,7,10

Everyday each rater will test one of the rater comparison vehicles.

Testing will proceed through the three phases as time and weather permit.

Phase I randomizes the order of fuel testing. The car fleet will be broken up into three groups, Red, Blue, and Yellow. The groups will have a mixture of all fuel system types. Raters will be permanently assigned to a vehicle. Phases II and III will test only one fuel per day. The test order will be as follows:

	DAY		CAR GROUP - FUEL	
PHASE I				
	1	RED 1	BLUE 5	YELLOW 9
	2	BLUE 2	YELLOW 6	RED 10
	3	YELLOW 3	RED 7	BLUE 11
	4	BLUE 8	YELLOW 12	RED 4
	5	RED 11	BLUE 1	YELLOW 4
	6	YELLOW 1	RED 8	BLUE 10
	7	BLUE 4	RED 2	YELLOW 7
	8	YELLOW 5	BLUE 3	RED 12
	9	RED 6	YELLOW 2	BLUE 7
	10	BLUE 12	RED 9	YELLOW 10
	11	RED 5	YELLOW 8	BLUE 6
	12	YELLOW 11	BLUE 9	RED 3

PHASE II

	DAY	<u>FUEL</u>	CAR GROUP		CAR GROUP	
	13	9	BLUE	YELLOW	RED	
	14	8	YELLOW	BLUE	RED	
	15	6	RED	YELLOW	BLUE	
	16	12	BLUE	RED	YELLOW	
	17	2	RED	BLUE	YELLOW	
	18	5	YELLOW	RED	BLUE	
	19	3	RED	YELLOW	BLUE	
	20	11	BLUE	YELLOW	RED	
PHASE III	21	10	YELLOW	BLUE	RED	
	22	1	YELLOW	RED	BLUE	
	23	4	BLUE	RED	YELLOW	
	24	7	RED	BLUE	YELLOW	

TEST SCHEDULE BRAINERD

The test plan will be broken down into three phases:

- I. 12 test days, all vehicles, all 12 fuels
- II. 8 test days, all vehicles, a repeat of fuels 1,3,5,6,7,9,10,12
- III. 4 test days, all vehicles, a repeat of fuels 2,4,8,11

Everyday each rater will test one of the rater comparison vehicles.

Testing will proceed through the three phases as time and weather permit.

Phase I randomizes the order of fuel testing. The car fleet will be broken up into three groups, Red, Blue, and Yellow. The groups will have a mixture of all fuel system types. Raters will be permanently assigned to a vehicle. Phases II and III will test only one fuel per day. The test order will be as follows:

	DAY		CAR GROUP - FUEL	
PHASE I				
	1	RED 1	BLUE 5	YELLOW 9
	2	BLUE 2	YELLOW 6	RED 10
	3	YELLOW 3	RED 7	BLUE 11
	4	BLUE 8	YELLOW 12	RED 4
	5	RED 11	BLUE 1	YELLOW 4
	6	YELLOW 1	RED 8	BLUE 10
	7	BLUE 4	RED 2	YELLOW 7
	8	YELLOW 5	BLUE 3	RED 12
	9	RED 6	YELLOW 2	BLUE 7
	10	BLUE 12	RED 9	YELLOW 10
	11	RED 5	YELLOW 8	BLUE 6
	12	YELLOW 11	BLUE 9	RED 3

PHASE II

	DAY	<u>FUEL</u>	CAR GROUP		
	13	6	BLUE	YELLOW	RED
	14	1	YELLOW	BLUE	RED
	15	10	RED	YELLOW	BLUE
	16	12	BLUE	RED	YELLOW
	17	9	RED	BLUE	YELLOW
	18	5	YELLOW	RED	BLUE
	19	7	RED	YELLOW	BLJE
	20	3	BLUE	YELLOW	RED
PHASE III	21	11	YELLOW	BLUE	RED
	22	8	YELLOW	RED	BLUE
	23	2	BLUE	RED	YELLOW
	24	4	RED	BLUE	YELLOW

APPENDIX E

PRELIMINARY REPORT ON THE 1988 CRC VOLATILITY PROGRAM ON THE EFFECT OF OXYGENATED FUELS AND ALTITUDE ON DRIVEABILITY AT LOW AMBIENT TEMPERATURES

COORDINATING RESEARCH COUNCIL

INCORPORATED

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SUSTAINING MEMBERS

American Petroleum Institute
Society of Automotive Engineers, Inc.

1988 CRC VOLATILITY PROGRAM ON THE EFFECT OF OXYGENATED FUELS AND ALTITUDE ON DRIVEABILITY AT LOW AMBIENT TEMPERATURES

(CRC Project No. CM-118-88)

MAY 1988

INTRODUCTION

The 1988 CRC driveability program investigated the effects of altitude and fuel oxygenates at low ambient temperature upon cold-start driveability with vehicles equipped with various fuel delivery systems. This program was conducted because of the use of gasoline-oxygenate blends to reduce ambient air carbon monoxide levels. The test program was divided into two phases. A high-altitude phase was conducted near Denver, Colorado, from January 11 through February 10, 1988, at an altitude of 5,486 feet; and a low-altitude phase was conducted in Brainerd, Minnesota, from March 4 through March 31, 1988, at an altitude of 1,226 feet. Test temperatures were 10°F to 40°F.

The test fleet of twenty-four vehicles (shown in Table I) was chosen to represent a variety of engines and fuel delivery systems. Fifteen of the vehicles were 1987 or 1988 models with closed-loop fuel metering systems. Included in this group were port-fuel-injected, throttle-body-injected, and carbureted vehicles. Six vehicles were pre-1980 open-loop carbureted vehicles. Three vehicles were used to develop rater correction factors.

The twelve test fuels consisted of three volatility levels of the following four fuel compositions: hydrocarbon-only; hydrocarbon plus 10 percent by volume ethanol (matched-volatility); hydrocarbon plus 11 percent by volume methyl tertiary-butyl ether (MTBE) (matched-volatility); and hydrocarbon plus 10 percent by volume ethanol (splash-blended). The term "matched-volatility" refers to a fuel which is targeted to have the same Reid vapor pressure and 10 and 50 percent distillation temperatures as the corresponding hydrocarbon-only fuel. These matched-volatility fuels had independent variation in the 10 and 50 percent distillation temperatures. The 90 percent distillation temperature was held constant for all the matched-volatility fuels. The term "splash-blended" refers to the addition of ethanol to the hydrocarbon-only fuels with no volatility adjustment. Specifications for the test fuels are shown in Table II.

The test procedure used in this program was the CRC Cold-Start and Warmup Driveability Procedure. Driveability malfunctions were recorded for the series of engine idles, accelerations and decelerations, and constant speed cruises over the first few miles of vehicle operation. Cold-start driveability malfunctions (hesitation, stumble, surge, backfire, stall, idle quality) were rated for severity. Each of the malfunctions was assigned a demerit level weighted for its relative importance; i.e., higher demerits indicate poorer driveability performance. Analysis of the data was based upon total weighted demerits (TWD's) as defined in the test procedure.

CONCLUSIONS

Analysis of the data provided the following conclusions:

- The altitude change between the two sites had no significant effect on driveability. For the fleet, demerits at high altitude were only 5 percent higher than at low altitude.
- Driveability performance decreased significantly with declining ambient temperatures. The temperature effect for the pre-1980 vehicles was about four times that found in current-model vehicles.
- The oxygenate-containing fuels evaluated performed significantly poorer than hydrocarbon-only fuels. Splash-blended ethanol (3.5 percent by weight oxygen) and matched-volatility MTBE (2 percent by weight oxygen) were not significantly different from each other, but were significantly poorer in performance than hydrocarbon-only fuels and significantly better in performance than matched-volatility ethanol blends. This effect occurred independently of vehicle type.
- \bullet The effect of volatility level was significant. As expected, increasing T_{10} and/or T_{50} gave poorer performance. This effect occurred independently of oxygenate.
- Within current-model vehicles, port-fuel-injected vehicles provided the best performance, followed by throttle-body-injected, and carbureted vehicles.
- The pre-1980 carbureted vehicles gave much poorer performance than current-model carbureted or fuel-injected vehicles. This difference was found to be highly significant.
- Within each vehicle group, large vehicle-to-vehicle variability in performance was found.

DATA SUMMARY

Statistical analysis of the data was used to quantify the results. The numerical values that were used to illustrate the effects of the experimental variables on vehicle driveability were statistically derived averages. This averaging was done over the levels of the other test variables using an analysis of variance technique at the 99 percent confidence level (p = 0.01). These values were based upon 1,073 valid tests, with TWD's adjusted to 25°F ambient air temperature.

The average TWD's were 133 at high altitude (5,486 feet) and were 127 at low-altitude (1,226 feet). This difference in TWD's is not significant (p = 0.40). One vehicle group tested, the current-model carbureted, had an average TWD at low altitude of 75 and at high altitude, an average TWD of 100. This effect, however, is inconclusive due to overall vehicle to vehicle variability (p < 0.15).

The average run temperatures for the high- and low-altitude phases of the program were $26.7^{\circ}F$ and $28.5^{\circ}F$, respectively, which were in good agreement with the mean target temperature of $25^{\circ}F$. All vehicle groups were responsive to test temperature. Over the range of $10^{\circ}F$ to $40^{\circ}F$, the temperature effect for the pre-1980 vehicles was a decrease of 4.9 TWD's per degree Fahrenheit increase in ambient temperature. The effect for the current-model vehicles was a decrease of 1.3 TWD's per degree Fahrenheit increase in temperature, which was significantly different from the pre-1980 vehicle effect (p < 0.01).

The average TWD's by oxygenate-type were:

Hydrocarbon-Only Fuels	-	110
11% Matched-Volatility MTBE	_	122
10% Matched-Volatility Ethanol	-	137
10% Splash-Blended Ethanol	-	118

The effect of vehicle type on these oxygenate-type averages was not significant.

For volatility-matched fuels, average TWD's were: 110 for hydrocarbon-only fuels; 122 for 11 percent by volume matched-volatility MTBE fuels; and 137 for 10 percent by volume matched-volatility ethanol fuels. These values were significantly different (p < 0.01).

Average TWD's were 137 for the 10 percent by volume matched-volatility ethanol fuels and 118 for the 10 percent by volume splash-blended ethanol fuels. These differences in demerits were significantly different (p < 0.01).

Average TWD's for the 10 percent by volume splash-blended ethanol fuels were 118. The splash-blended ethanol fuels performed significantly poorer (p < 0.01) than the hydrocarbon-only fue: (TWD's = 110).

Volatility-adjusted MTBE blends were not significantly different from splash-blended ethanol (p < 0.01).

The twelve test fuels were classified into three volatility levels. Target T_{10} values were 110°F and 140°F; target T_{50} values were 200°F and 230°F. The combinations tested and the average TWD's were:

T ₁₀	T ₅₀	TWD	
Low	Low	105	
Low	High	125	
High	High	163	

All differences were significant (p < 0.001). This occurred independently of oxygenate. As expected, increasing T_{10} and/or T_{50} gave poorer performance.

The average TWD's within the vehicle groups were:

Port-Fuel-Injected	_	50
Throttle-Body-Injected	-	75
Current-Model Carbureted	-	86
Pre-1980 Carbureted	-	363

The difference between the port-fuel-injected vehicles and current-model carbureted vehicles was significant at the 93 percent confidence level (p < 0.07). The differences between all current-model vehicles and pre-1980 vehicles were highly significant (p < 0.0001).

Members of the 1988 CRC Volatility Analysis Panel:

Ρ.	Α.	Yaccarino, Leader	General Motors Research Laboratories
D.	A.	Barker	Shell Development Company
J.	н.	Baudino	AutoResearch Laboratories, Inc.
J.	Ρ.	Graham	Chevron Research Company
		Painter	Consultant
R.	M.	Reuter	Texaco Inc.
		Schanerberger	Ford Motor Company
		Steinke	Sun Refining and Marketing Company
		Steury	Amoco Oil Company
L.	J.	Sumans ky	Mobil Research and Development Corp.
C.	Τ.	Valade	Chrysler Corporation

TABLE I

TEST VEHICLES

Model Year	Make/Model	Displacement, Liters	Fuel System		
1987	Chevrolet Caprice	5.0	Carbureted		
1987	Plymouth Horizon	2.2	Carbureted		
1987	Chrysler Fifth Avenue	5.2	Carbureted		
1987	Honda Civic	1.5	Carbureted		
1987	Ford Escort	1.9	Carbureted		
1987	Nissan Sentra	1.6	Carbureted		
1988	Chevrolet Astro	4.3	Throttle-Body-Injected		
1987	Mercury Cougar	3.8	Throttle-Body-Injected		
1987	Chrysler LeBaron	2.5	Throttle-Body-Injected		
1987	Buick Century	2.5	Throttle-Body-Injected		
1987	Buick LeSabre	3.8	Port-Fuel-Injected		
1987	Ford Aerostar	3.0	Port-Fuel-Injected		
1987	Ford LTD Crown Victoria	5.0	Port-Fuel-Injected		
1987	Chrysler LeBaron (turbo)	2.2	Port-Fuel-Injected		
1987	Toyota Camry (four-valve)	2.0	Port-Fuel-Injected		
1978	Dodge Van	5.9	Carbureted		
1979	Ford Fairmont	2.3	Carbureted		
1979	Plymouth Volare	5.2	Carbureted		
1979	Dodge Pickup Truck	5.9	Carbureted		
1979	Pontiac LeMans	3.8	Carbureted		
1979	Ford Van	5.0	Carbureted		
Rater Comparison Vehicles:					
1987	Dodge Charger	2.2	Carbureted		
1987	Toyota Camry (four-valve)	2.0	Port-Fuel-Injected		
1987	Buick Century	2.5	Throttle-Body-Injected		

TABLE II

TEST FUEL DESIGN LEVELS

<u>Fuel</u>	10% Dist.	50% Dist.					
HYDROCARBON-ONLY							
1	110	200					
1 2 3	110	230					
3	140	230					
HYDROCARBON + 10 VOL.% ETHANOL (Volatility-Matched)							
4	110	200					
5 6	110	230					
6	140	230					
HYDROCARBON + 11 VOL. # MTBE (Volatility-Matched)							
7	110	200					
8 9	110	230					
9	140	230					
HYDROCARBON + 10 VOL.% ETHANOL (Splashed)							
10	Fuel 1 with 10% Ethanol						
11	Fuel 2 with 10% Ethanol						
12	Fuel 3 with 10% Ethanol						

Fuels 1 through 9 shall have a 330°F 90% distillation temperature. Tolerances shall be +5°F on distillation temperatures. Minimum delta T_{10} and T_{50} values are also specified as follows:

- I₁₀ for Fuel 3 shall be at least 25°F higher than Fuels 1 and 2.

- b) The for Fuel 3 shall be at least 25°F higher than Fuels 1 and 2.

 b) The for Fuel 6 shall be at least 25°F higher than Fuels 4 and 5.

 c) The for Fuel 9 shall be at least 25°F higher than Fuels 7 and 8.

 d) The for Fuels 2 and 3 shall be at least 25°F higher than Fuel 1.

 e) The for Fuels 5 and 6 shall be at least 25°F higher than Fuel 4.

 f) The for Fuels 8 and 9 shall be at least 25°F higher than Fuel 7.

 RVP ranges for all fuels are specified below:

1, 2,
$$\frac{\text{Fuel}}{4, 5}$$
, 7, 8, $\frac{\text{RVP, psi}}{13.5 \pm 0.5}$ Maximum possible with T_{10} @ 140°F

All fuels shall be unleaded and have a minimum (R+M)/2 octane rating of 88. Fuels shall exhibit no phase separation at 0°F. Fuels shall contain no more than 3% Benzene.

Fuels shall not exceed the ASTM maximum endpoint specification of 437°F.

Fuels shall not contain more than 40% aromatic.

Fuels shall contain an antioxidant and a corrosion inhibitor.

Ethanol shall be denatured with unleaded gasoline (CDA Formula #20).

APPENDIX F INDIVIDUAL LABORATORY FUEL PROPERTY DATA

RESULTS OF ANALYSES FOR THE 1988 CRC DRIVEABILITY PROGRAM FUELS

. APPENDIX F

Individual Laboratory Results

		₽ņ		:		Fuel	- 2			Fue	က	Í		Fue	*	
Leb	-4	74	ભ	41	-4	ત્ય	ଜା	41	-	2	ଜା	⊲ I	-4	coli	ભા	∢i
RVP, psi	12.6	13.4	14.0	13.6	13.1	13.8	13.6	13.7	ø.	16.4	9.	10.1	13.4	14.0	13.6	13.7
Dist, % Evap. @ oF IBP	œ 4		82	78	82	,	89	92	80	•	96	88	**	1	œ 4	82
S vol.%	66	•	•	•	26	ı	1	1	120	1	1	•	164		• ;	• {
10 vo.	112	107	110	198	110	186	196	116	143 28	134	144	133	114	169	116	108
	156	149	149	147	163	162	160	167	200	205	202	200	140	141	143	143
	174	174	172	171	198	198	196	202	222 235	222 228	223 238	219 232	160	156 286	167 198	159 208
R 0 > 00	230	231	236	229	264	261	264	289 289	250 250	251 251	251 251	247	248	242	245	240
	270	268	273	286	288	286	296	282	278	274	278	270	266	262	268	264
	313	307	316	368	310	306	312	311	310	308	313	306	286	294	297	302
	337	334	344	340	330	326	336	338	328	326	334	329	334	326	333	326
	351	356		•	348	346	•	•	340	344	•	•	344	342	•	1
EP	383	392	405	386	392	391	358	391	384	372	394	386	382	377	392	378
T(V/L)=20, °F	ı	110	118	•	1	120	120	ı	•	147	146	•		113	116	ŧ
FIA, X		į			,	9	ŝ			č	ć		č	ċ	ć	
Aromatics 01-41-	9	77	R (:	ę °	9	70		9 °	٦ °	? «		† ¢	,	R C	• 1
Saturates	93	70	9 0		61	200	‡		91	9 9	, 4	•	61	70	68	1
Oxygenate Content, % Ethanol MTBE	.0 9.0	66.1 1.6	<6.1 1.6	1 1	<0.1 1.6	<0.1 1.0	46.1	t 1	<6.1 1.3	1.3	<0.1 1.5		9.0		1.6	1 1

APPENDIX F (Continued)

Results of ANALYSES FOR THE 1988 CRC DRIVEABILITY PROGRAM FUELS Individual Laboratory Results

		Fuel	9			π ⊕	6			A D	7			Œ.	α -	
Teb Teb	-4	CAI	ભા	41	-4	CAS	м	41	-4	CO#	M	41	-	~1	1	41
RVP, psi	12.8	13.6	13.4	13.3	4.	16.2	89 80	9.	13.6	13.8	14.3	13.8	12.8	13.1	13.8	13.7
Dist, % Evap. 6 oF 18P	8	1	œ 4	60 60	6	•	164	Q.	48	ı	82		œ	ı	o o	;
8. lov 8	106	•	,		129	•	1	3 ,	168	1	· .	: ,	6		2 1	٠,
	118	113	116	111	146	140	142	142	112	107	101	103	112	104	111	102
	136	132	134	131	152	156	156	156	130	127	126	123	136	130	133	127
6 K 0 > 0 4	171	1 4 % 1 0 4 %	162	147	216	168 214	172 22 6	170 206	150	148	144	145	162	167	162	163
	226	232	240	234	240	236	239	236	208	205	200	200	232	229	231	222
	264	258	261	255	250	248	262	251	236	236	233	231	258	255	269	262
	278	278	280	276	268	266	270	289	270	284	285	282	277	275	281	278
₩. o > 0 0	300	366	308	302	364	297	302	297	313	308	313	307	303	299	308	300
	337	329	338	336	331	328	339	330	342	336	347	343	330	326	333	328
%: o > 96	347	346	•		348	342	1		358	358	•	•	347	342	•	
a	383	376	382	383	382	382	394	387	405	397	408	397	387	380	388	386
T(V/L)=20, oF	•	116	118	ı	1	136	149		ı	119	118	1	•	124	121	1
FIA, %																
Aromatics 01.5:1	ဗ	27	58		41	34	38	1	38	31	32		38	28	36	1
	7	~	-	1	8	N	m	1	8	~	8	ı	~	~	ო	,
Settle tes	9	71	71		29	6	69	1	86	67	88	1	63	69	61	•
Oxygenate Content, X																
Ethanol	8	9.5	8.7		9.3	9.6	6.6	1	<0.1	<0.1	(0.1		<0.1	<0.1	(0.1	ı
MISE	T: T	6.7	6.7	ı	.	8.	6.0	1			11.2	ı		10.5	10.6	1

APPENDIX F (Continued)

RESULTS OF ANALYSES FOR THE 1988 CRC DRIVEABILITY PROGRAM FUELS

Individual Laboratory Results

	į	Fuel	6			Fuel	1 10		į	Fuel	111			FU	Fuel 12	Î
Lab	4	ભા	mi	41	—	71	mi	41	-4	%	ભ	∀ I	- 4	64	어	→ I
RVP, psi	9.	6	9.6	.	13.6	14.2	14.0	13.7	13.2	13.8	13.4	13.4	16.3	11.0	10.5	16.8
Dist, % Evap. @ oF IBP	8	1	88	88	88	ı	98	78	8	1	88	83	83	•	86	83
6 vol.x	126	•		•	106	•	•		106		•		120	1	•	
	146	138	142	139	112	101	111	106	114	112	114	109	137	129	134	131
26 vol. X	176	172	173	172	126	120	123	121	132	129	131	128	147 158	147 158	148	148
4	218	218	216	216	146	144	146	146	167	156	156	167	190	182	186	173
	234	234	234	233	176	164	174	165	188	197	183	194	226	222	226	224
	248	250	248	247	218	214	221	198	248	242	248	239	248	243	243	240
7. lov 87	268	268	268	266	261	254	282	236	274	273	275	271	288	288	288	282
	302	299	306	298	300	366	314	302	300	299	308	299	304	298	310	301
	332	328	336	330	336	330	342	334	328	324	330	327	329	324	332	328
	347	351	•	•	349	348	1	•	344	343	•	1	340	338		ı
E B	286	386	354	382	388	386	398	382	388	387	403	386	384	377	394	380
T(V/L)=26, oF	1	147	148	ſ	1	111	116	ı	1	114	117	1	1	128	139	1
FIA, %	!	,	:		,	,	,		!	;	9			;	;	
Aromatics	38	33	41	•	36	58	32	•	42	32	42	ı	90 P3	31	32	•
010111	8	8	ო	ı	~	~	ო	•	8	ო	4		4	ო	m	1
Saturates	69	98	20	r	82	70	99	1	28	62	2 4	1	28	99	99	1
Oxygenate Content, % Ethanol MTBE	<0.1 11.0	<0.1 11.5	<6.1 11.4	1 1	7.7	8 9. 1.	7.9	1 1	4.0	16.1	9.8		9.7	8 2	16.1	1 1

APPENDIX G RAW DATA

GLOSSARY FOR RAW DATA

FUEL = Fuel Number VEH = Vehicle Number

RUN = Chronological Test Day

RATER = Designation for Individual Rater

<u>Temperatures</u>

SOAK = Overnight Soak Temperature

RUN = Ambient Temperature at Beginning of Individual Test

TNK1 through TNK7 =

Fuel Tank Temperatures Taken at Seven Times During Cold-

Start and Driveaway Cycle

Malfunctions

HES = Number of Hesitation Demerits During Cold-Start and

Driveaway Cycle

STUM = Number of Stumble Demerits During Cold-Start and

Driveaway Cycle

SRG = Number of Surge Demerits During Cold-Start and Driveway

Cycle

BKFR = Number of Backfire Demerits During Cold-Start and

Driveaway Cycle

ACL STL = Number of Acceleration Stall Demerits During Cold-Start

and Driveaway Cycle

DCL STL = Number of Deceleration Stall Demerits During Cold-Start

and Driveaway Cycle

INIT START = Number of Initial Starting Demerits During Cold-Start and

Driveaway Cycle

RSTRT1 through RSTRT3 =

Number of Restarting Demerits (for first three weeks)

During Cold-Start and Driveaway Cycle

IDL NEUT RUF= Number of Idle Demerits in Neutral Gear During Cold-Start

and Driveway Cycle

IDL NEUT STL= Number of Stall Demerits While Idling in Neutral Gear

During Cold-Start and Driveaway Cycle

IDL DRY RUF = Number of Idle Demerits in Drive Gear During Cold-S'art

and Driveaway Cycle

IDL DRY STL = Number of Stall Demerits While Idling in Drive Gear During

Cold-Start and Driveaway Cycle

CLD TWD = Total Weighted Demerits for Cold-Start and Driveaway Cycle

WRM TWD = Total Weighted Demerits for Warmed-up Cycle

SUMMARY OF COLD DEMERITS BY CRITERIA - DENVER

- DENVER
•
CRITERIA
¥
DEMERITS
OF COLD
SUMMARY

76 76	99	100	53	20	7 2	761		2 6	30,	284	122	99	194	123	2 :	- (ν α	٠ =	127	236	146	48	26	3 5	61	36	292	250	148	70	, ,	80	22	402	223	7, 7	159	7.	98	102	104	54	398	379
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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - DENVER

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - DENVER

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - DENVER

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - DENVER

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - DENVER

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - DENVER

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - BRAINERD

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - BRAINERD

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - BRAINERD

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SUMMARY

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SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - BRAINERD

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8 66 3 3/25/88 32 36 35 37 38 38 40 41 42 2 94 61 49 22 8 6 9 66 3 3/25/88 32 36 35 27 28 30 31 49 66 3 3/19/88 17 25 0 0 0 0 4 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 </td <td>75</td> <td></td> <td></td> <td>3/19/88</td> <td>17</td> <td>52</td> <td>c ;</td> <td>22</td> <td>23</td> <td>24</td> <td>25</td> <td>56</td> <td>27</td> <td></td> <td></td> <td></td> <td>53</td> <td></td> <td>20</td> <td>20</td> <td>355</td> <td>66</td> <td>454</td>	75			3/19/88	17	52	c ;	22	23	24	25	56	27				53		20	20	355	66	454
9 60 3 J/19/88 1 1/2 25 27 28 30 32 0 31 7 7 0 1 7 0 0 0 4 25 13 1 7 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 </td <td>2 :</td> <td></td> <td></td> <td>3/25/88</td> <td>32</td> <td>9 ;</td> <td>35</td> <td>37</td> <td>80</td> <td>38</td> <td>0 7</td> <td>41</td> <td>7.5</td> <td></td> <td></td> <td></td> <td>6 7</td> <td></td> <td>*</td> <td>. و</td> <td>902</td> <td>9.</td> <td>242</td>	2 :			3/25/88	32	9 ;	35	37	80	38	0 7	41	7.5				6 7		*	. و	902	9.	242
9 66 3 3/25/88 32 36 33 33 34 35 36 38 1 25 13 6 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 </td <td>21</td> <td></td> <td></td> <td>3/19/88</td> <td>1</td> <td>52</td> <td>0</td> <td>25</td> <td>25</td> <td>27</td> <td>28</td> <td><u>0</u></td> <td>32</td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td>C</td> <td>-</td> <td>89</td> <td>æ</td> <td>9 :</td>	21			3/19/88	1	52	0	25	25	27	28	<u>0</u>	32				_		C	-	89	æ	9 :
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15 66 3 3/25/88 32 35 33 33 34 35 37 12 28 32 14 14 8 8 16 56 1 3/25/88 24 37 30 31 32 33 34 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 36 <t< td=""><td>12</td><td></td><td></td><td>3/09/88</td><td>24</td><td>36</td><td>0</td><td>0</td><td>c</td><td>0</td><td>0</td><td>O</td><td>c</td><td></td><td></td><td></td><td>20</td><td></td><td>œ</td><td>2</td><td>96</td><td>17</td><td>113</td></t<>	12			3/09/88	24	36	0	0	c	0	0	O	c				20		œ	2	96	17	113
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18 66 3 3/25/88 32 35 33 34 34 37 36 40 40 1 26 4 1 7 1 0 1 1 9 54 1 3/09/88 24 37 32 31 32 33 36 38 41 4 14 25 1 1 1 1 1 1 1 1 9 66 1 3/25/88 32 35 36 36 36 37 38 39 40 8 4 2 2 2 2 2 2 2	1.2			3/09/88	24	33	c	0	C	С	c	0	c	-			51		-	61	121	5.5	176
19 54 1 3/09/88 24 37 32 31 32 33 36 38 41 4 14 25 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.2			3/25/88	32	35	33	3,4	3,4	11	36	07	۷0	-			-		-	0	3.2	œ	40
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Free 10

SUMMARY OF COLD DEMERITS BY DRIVING CYCLE - BRAINERD

MAKE		TOTAL		528	415	25	19
		0 1 2 3 4 5 6 0->3 4->6	<u>ИНБИНИНИЕВЕВИНЕВЕВИНИВИНИНИНИНИНИНИНИНИНИНИ</u>	198	159	_	ę
	ARETHUBERED BRIVING CYCLE RESIDENCE	0->3	HMMMMM	330	256	7	\$\$
	F.	ş	HMMH	49	43	0	7
	CYC!	2		67	19	0	~
	IV INC	4		82	64	-	7
	FO	٠	MANA	74	74	0	2
Ī		7	MANAM	80	9,	54	98
	# F # # #.	_	MAKE	128	64	97	26
	,	c	MMMM	48	42	-	-
		TNK 7	HAMMH	9/	99	20	43
	# # # # # # # # # # # # # # # # # # #	TNK6	MHHH	74	55	41	0%
	TEMPERATURES ====================================	RUN INK! INK2 INK3 INK4 INK5 INK6 INK7	HHHM	65	55	44	38
	RES =	TNK4		28	43	40	11
	ERATI	TNK3		20	4 2	38	36
		TNK2	RAMME	45	35	36	34
		INKI	FEMME	37	35	35	33
	10 10 10 10 10 10 10 10 10 10 10 10 10 1	RUN	THE STATE	37	35	37	35
		SOAK	-		32	24	32
MANANANANANANANANANANANANANANANANANANAN		FUEL VEH RUN RATER DATE	HERRICH HERRICH STATES	3/09/88	3/25/88	3/09/88	3/25/88
		ATER	HATER	7	7	<u>_</u>	~
		RUN R	THE CAN	54	99	54	99
Ī		VEH	FIFFER	12 20 54	99 02	21	71
		FIFT	MAMM	7	1.2	12	~

APPENDIX H SAS PROGRAM, CODE, AND OUTPUT

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC.
THIRD PASS AT GLM

GENERAL LINEAR MODELS PROCEDURE

CLASS LEVEL INFORMATION

- SA NEWCARB NEWPFI NEWTBI OLDCARB BRAINERD DENVER VALUES LEVELS VEHGRP CLASS SITE

ETOH ETOH_S HC MTBE

Λ×ο

VOLATIL

NUMBER OF OBSERVATIONS IN DATA SET = 938

NOTE: ALL DEPENDENT VARIABLES ARE CONSISTENT WITH RESPECT TO THE PRESENCE OR ABSENCE OF MISSING VALUES. HOWEVER, ONLY 937 OBSERVATIONS CAN BE USED IN THIS ANALYSIS.

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC. THIRD PASS AT GLM

GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: SQRTCOLD

SOURCE	OF	SUM OF SQUARES	MEA	MEAN SQUARE	F VALUE
MODEL	06	27695.64249005	307.	307.72936100	131.16
ERROR	846	1984.84466517	2.	2.34615209	PR v F
CORRECTED TOTAL	936	29680.48715523	<u>-</u>		0.0001
R-SQUARE	c . v .	ROOT MSE	SQRTC	SQRTCOLD MEAN	
0.933126	13.4028	1.53171541	=	11.42836307	
SOURCE	0F	TYPE IV SS	F VALUE	PR > F	
RUNTEMP	-	456.59185143	194.61	0.0001	
RUNTEMP * VEHGRP	က	39.57982910	5.62	0.0008	
VEHICLE (VEHGRP)	17	2532.26261962	63.49	0.0001	
SITE	-	18.17499910	7.75	0.0055	
SITE * VEHICLE (VEHGRP)	50	481.51019018	10.26	0.0001	
OXY	က	180.86151943	25.70	0.0001	
VOLATIL	2	1051.99696983	224.20	0.0001	
VEHIC+VOLAT (VEHGR)	40	325.46445954	3.47	0.0001	
VEHGRP	၉	20521.71395802	2915.66	0.0001	

PARAMETER	ESTIMATE	T FOR HO: PARAMETER=O	PR > [T]	STD ERROR OF ESTIMATE	
INTERCEPT	21.12692283 B	45.58	0.0001	0.46354602	
RUNTEMP	-0.12919879 B	-10.73	0.0001	0.01204046	
RUNT EMP * VEHGRP	NEWCARB				
	0.03326254 B	1.86	0.0634	0.01789142	
	NEWPFI				
	O.06815899 B	3.89	0.0001	0.01751563	
	NEWTBI				
	0.05165611 B	2.94	0.0034	0.01758040	
	OLDCARB				
	0.00000000 B	•	•	٠	
VEHICLE (VEHGRP)	3 NEWCARB		·		
	-10.02296075 B	-15.72	0.0001	0.63742224	
	7 NEWCARB				
	-7.08243994 B	~ 10.83	0.0001	0.65370384	
	11 NEWCARB				
	-7.70199818 B	-12.09	0.0001	0.63684093	
	15 NEWCARB				
	-9.80374995 B	-15.32	0.0001	0.64011285	
	19 NEWCARB				
	-11.78008713 B	- 18 ,27	0.0001	0.64491734	
	2 NEWPFI				
	-11,52537962 B	- 18.09	0.0001	0.63713664	

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC.
THIRD PASS AT GLM

GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: SORTCOLD

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PARAMETER	ESTIMATE	T FOR HO: PARAMETER=O	PR > [T]	STD ERROR OF ESTIMATE
	-12.03601057 B	- 18 . 89	0.0001	0.63712568
		-26.84	0.0001	0.63811045
		- 18 . 34	0.0001	0.63722766
	18 NEWPFI -13,41432374 B	-20.92	0.0001	0.64136198
		-15.45	0.0001	0.63675905
		-18.46	0.0001	0.63675719
		-14.14	0.0001	0.63681960
		-19.32	0.0001	0.64178874
	21 NEWIBI -9.65161158 B	-14.98	0.0001	0.64421157
	4 OLDCARB -1.10527353 B	-1.74	0.0824	0.63568092
	6 OLDCARB 3.58490363 B	5.66	0.0001	0.63391982
		- 1.89	0.0595	0.63728722
	12 OLDCARB -2.36410222 B	-3.72	0.0002	0.63619043
-		-1.53	0.1273	0.63140425
SITE	0.00000000 B	•		
1	1.68806596 B	3.68	0.0002	0.45868965
	8		•	•
SITE *VEHICLE (VEHGRP)	BRAINERD 3 NEWCARB -2.23024129 B	-3.44	9000	0.64881797
	BRAINERD 7 NEWCARB		 	
	-5.63170665 B	8.59	0.0001	0.65564327
		-3.58	0.0004	0.64889144
	BRAINERD 15 NEWCARB -0.89121060 B	-1.37	0.1702	0.64916763
	BRAINERD 19 NEWCARB	6, 6	0.00	
	DENVER 3 NEWCARB	<u> </u>	58.0	0.63280330
	O.OOOOOOOO B DENVER 7 NEWCARB		•	
	O.OOOOOOOO B DENVER 11 NEWCARB		•	

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC. THIRD PASS AT GLM

O SENVER	.00000000 B			
0				
DENVER O.	19 NEWCARIS			
BRAINERD	2 NEWPFI			
-2-	. 13083404 B	-3.28	0.0011	0.64876153
DRAINERO -2.	34249516 B	-3.61	0.0003	0.64919855
BRAINERD	10 NEWPFI			
. 1 -	.21009156 B	-1.85	0.0647	0.65413508
DAMINERO -2.	38221435 B	-3.67	0.0003	0.64882034
BRAINERD	18 NEWPFI		! ! !	
OENVED	.95068302 B	1.47	0.1432	0.64876579
DENVER O.	.00000000 B	•		
DENVER	S NEWPFI			
DENVER O	10 NEWPFI			
0	$^{\circ}$		•	
DENVER	14 NEWPFI			
OFNVED O	.00000000 B	٠.		
0	.00000000 B	. •		
BRAINERD	1 NEWTBI			
.1-	63	-2.87	0.0042	0.64937151
DRAINERU -2	9 NEWIBL	-3.16	0.0016	0.64896036
BRAINERD	13 NEW181))))	
-	(-)	-1.89	0.0598	0.64900814
BRAINERD	17 NEWTB1	,	,	1
	.51088316 B	-2.33	0.0201	0.64874244
BRAINERD -3	21 NEWTBI	70	5	0 64864304
DENVER	1 NEWTBI	2	-	100.00000.00
0	8			
DENVER	9 NEWTBI			
O.	.00000000 B			·
0	. 00000000 B			
DENVER	17 NEWTBI			
OFNVED O	.00000000 B			
0.	\sim			•
BRAINERD	4 OLDCARB			
Ť.	94	-1.82	0.0691	0.65597456
BRAINERD	œ	,	,	
RRATNFRO	. /3483424 B	16.41	5	0.64844311
-	ခ	-2.04	0.0414	0.65133967
BRAINERD	CAR	-		
O-	.30582452 B	-0.47	0.6391	0.65185334
-2.	8	-3:85	0.0001	0.64840295
BRAINERD	20 OLDCARB			

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & DXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC. THIRD PASS AT GLM .

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							4.69 0.0001 0.14358196	-1 42 0 1547 0 14083716	 -3.86 0.0001 0.14585918		-5.70 0.0001 0.55242057	0.0013		-0.52 0.6030 0.78157455	0.16 0.8703 0.80630987		0.02 0.9866 0.78813702	0.75 0.4523 0.82004762		0.23 0.8213 0.78009106	-1.44 0.1500 0.80524218))))		1 56 0,1185 0.78125321	. 	1.29 0.1975 0.81613349			0.94 0.3476 0.78713139	-0.49 0.6239 0.82024387		•	2.45 0.0143 0.78171020
0.00C00000 B DENVER 4 0LDCARB 0.00000000 B DENVER 6 0LDCARB	0 8 8	9.5	ó	DENVER 16 OLDCARB	DENVER 20 OLDCARB	0.0000000 B	0.67308590 B	ETOH_S -0 20060578 B	-0.56254583 B	MIBE O COCOCOCO B		-1.86237170	2 0.00000000 B 3 0 NEWCARB	•	3 2 NEWCARR	٧.	O.01321903 B		11 O NEWCARB		11 1 NEWCARB -1.16022630 B		(15 U NEWCARB 1.22080695 B		1.05159509 B	•	,	O.73972271 B 19 1 NEWCARB		19 2 NEWCARB		1.91846922 B
						XXU					VOLATIL		VEHIC * VOLAT (VEHGR)																				

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC. THIRD PASS AT GLM

GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: SORTCOLD

PARAMETER

STD ERROR OF ESTIMATE	0.80574781			0 78143422		0.80580750			0 78013647		0.81431404			0.78023383	0000	0.80324041			0.78096797	5 8 14 0 2 2 3	000000000000000000000000000000000000000			0.78196619		0.80535072			0.78025413		0.80529069			0.78017532		0.80553225			0.78139902	
PR > [T]	0.0465	1		8001		0.2018			0.0742	!	0.9014			0.0430	0	0.3000	•		0.0010	0 2003	0.70			0.6300		0.9940			0.6085	1	0.2177	•	•	0.0215		0.1566	,	•	0.0001	
T FOR HO: PARAMETER=O	1.99			. 63		1.28		٠	1 79		-0.12		••	2.03		0.6	•		3.30	96.		•		0.48		-0.01			-0.51		-1.23	٠	•	-2.30		-1.42		•	5.13	
ESTIMATE	NEWPF1 1.60672953 P		0.00000000 B	NEWPF1 1 27612097 E		1.02944139 B		0.00000000 B	NEWPF1 1 39448824 R		-0.10092587 B	NEWPF I		1.58140033 B		0.54329/51 B	0.0000000 B		2.57353299 B	NEWPFI		0.CO000000 B		0.37685124 B		-0.00601756 B	0.0000000 B		-0.39981085 B		-0.99340347 B	0.00000000 B		-1.79726853 B		-1.14206786 B	NEW I BI		4.01050890 B NEWTBI	
	-	Q	,	0	-		7		0	-		7	0		-	•		0		~	~		0		-	c	٧	0		-	•	N	0		-		7	0	-	
	2	8	•	ភ	ß		r.	•	2	5	•	10	4		4	•	<u>-</u>	18	•	80	ά.		-		-	•	-	6		o O	Ċ	n	13		13	•	.	17	17	

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC. THIRD PASS AT GLM

1.86 0.0625 0.81588253		0.23 0.8185 0.78156271	0,77 0.4412 0.81637881	n'	0.66 0.5069 0.79868020	0 2660 0 2680 0 111			-0.41 0.6823 0.78464399	0 12 0 9052 0 79844274	0.3032		-1.51 0.1304 0.78065994	0.61 0.5432 0.81944885		0362367 0 6367 0 61 0	200	0.25 0.8036 0.81070452		0.67 0.5054 0.77883802	0.92 0.3589 0.79408969									
1.52158646 B	17 2 NEWTBI	•	21 1 NEWIBI 0.62901922 B	21 2 NEWTBI		4 1 OLDCARB	0.88294708 B			6 1 OLDCAR3		8 O OLDCARB	•	8 1 ULUCARE 0.49841549 B	8 2 OLDCARB	12 O ULDCAKB	12 1 DLDCARB	•	16 O OLDCARB		16 1 ULUCARE O.72899560 B	O COCCOCCO B)	0.0000000 B	20 2 ULUCARE 0.00000000 B	NEWCARB	NEWPFI	0.0000000 P	NEW B1	

VEHGRP

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & DXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC.
THIRD PASS AT GLM

GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: SQRTCOLD

NOTE: THE X'X MATRIX HAS BEEN DEEMED SINGULAR AND A GENERALIZED INVERSE HAS BEEN EMPLOYED TO SOLVE THE NORMAL EQUATIONS. THE ABOVE ESTIMATES REPRESENT ONLY ONE OF MANY POSSIBLE SOLUTIONS TO THE NORMAL EQUATIONS. ESTIMATES FOLLOWED BY THE LETTER B ARE BIASED AND DO NOT ESTIMATE THE PARAMETER BUT ARE BLUE FOR SOME LINEAR COMBINATION OF PARAMETERS (OR ARE ZERO). THE EXPECTED VALUE OF THE BIASED ESTIMATORS MAY BE OBTAINED FROM THE GENERAL FORM OF ESTIMABLE FUNCTIONS. FOR THE BIASED ESTIMATORS HO: E(BIASED ESTIMATOR) = O. ESTIMATES NOT FOLLOWED BY THE LETTER B ARE BLUE FOR THE PARAMETER.

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & DXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC. THIRD PASS AT GLM

GENERAL LINEAR MODELS PROCEDURE

LEAST SQUARES MEANS STANDARD ERRORS AND PROBABILITIES CALCULATED USING THE TYPE IV MS FOR SITE*VEHICLE(VEHGRP) AS AN ERROR TERM

PROB > |T| HO: LSMEAN1=LSMEAN2 SORTCOLD LSMEAN

0.3952 11.2599419 BRAINERD

DENVER

PROB > |T| HO: LSMEAN(1)=LSMEAN(J) 7 LSMEAN SORTCOLD λ×ο

0.0001 0.0001 0.0001 0.0111 0.0001 0.000 0.0001 10.8398673 11.7135590 11.0404731 ETOH_S ETOH MTBE TO ENSURE OVERALL PROTECTION LEVEL, ONLY PROBABILITIES ASSOCIATED WITH PRE-PLANNED COMPARISONS SHOULD BE USED NOTE:

STANDARD ERRORS AND PROBABILITIES CALCULATED USING THE TYPE IV MS FOR VEHIC*VOLAT(VEHGR) AS AN ERROR TERM

PROB > |T| HO: LSMEAN(I)=LSMEAN(J) 1/J 1 2 3 SORTCOLD LSMEAN VOLATIL

0.0001 0.0001 0.0003 0.0001 0.0003 10.2398814 11, 1938851 0

NOTE: TO ENSURE OVERALL PROTECTION LEVEL, ONLY PROBABILITIES ASSOCIATED WITH PRE-PLANNED COMPARISONS SHOULD BE USED.

STANDARD ERRORS AND PROBABILITIES CALCULATED USING THE TYPE IV MS FOR VEHICLE(VEHGRP) AS AN ERROR TERM

PROB > |1| HO: LSMEAN(I)=LSMEAN(\cup) I/ \cup 1 2 3 4 SORTCOLD LSMEAN VEHGRP

0.000.0 0.0001 0.5922 0.1821 0.0001 0.0001 0.0702 0.1821 0.5922 0.0702 9.2973184 7.0543624 8.6643523 19.0557934 NEWCARB OLDCARB NEWPF I NEWTBI

NOTE: TO ENSURE OVERALL PROTECTION LEVEL, ONLY PROBABILITIES ASSOCIATED WITH PRE-PLANNED COMPARISONS SHOULD BE USED

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS
ANALYSIS FOR FUEL, SITE EFFECTS, ETC.
THIRD PASS AT GLM
OBSERVED & RESIDUALS VS. FITTED RESULTS - COLD TWD

ETC.
OBS.
7
11
8
088.
-
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⋖
LEGEND:
SQRTCOLD*PSQRTCLD
9
PLOT

	•	A A AA A AAA A AAAA A AAAA A AAAA A AAAA	77 DA DA A A A A A A A A A A A A A A A A	BEBC BBB BBBA BBBA	AC A BA AADA ABBC	BAB ABA ABAA	A AAAAAA B BAAAAA	CAAAEBBA B BEBOBDADE	A A E CCEEDD BB A A A A A A CDBBFNEDA A A CDLINEHADAB	B ACHKGFBECB A A . A A BCAGDLUCC B BDAHECHIGFC A	404	CB DCDACA BCA ACAC B AA C CA A ACC A	38 A A A B B A A B B A A B B A A B A A B A B A B A B B B B B B B B B B B B B B B B B B B B	A A	10 12 14 16 18 20	PSQRTCLD
												AA BA ACC	ACBBAA ABA B A B	A A		
27.5 +	25.0		22.5	50.0	z. +	15.0	SQRTCOLD	12.5	10.0	7.5	•	+		+ 0.0	0	

1 OBS HAD MISSING VALUES

NOTE:

CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS ANALYSIS FOR FUEL, SITE EFFECTS, ETC.
THIRD PASS AT GLM
OBSERVED & RESIDUALS VS. FITTED RESULTS - COLD TWD

LEGEND: A = 1 08S, B = 2 08S, ETC. PLOT OF RSQRICLD*PSQRICLD

RSGRTCLD 6	_+-				∢										
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4	+-				4 •	۷ ∢				4	∢				
ю	+-		< <	4	4 4 8	ABAD A	⋖	4	⋖	4 4	4 4 8	∢			
8	+_	æ	4 A A A A A A A A A A A A A A A A A A A	A A A A A A	CBACAA C AB CE BAA B B/	A CBACAA B C AB CBA ABAA B BAAAA	4 4 4 4	∀ 89		A AA A A A A A A A A A A A A B A B A B	A B BA A B BA	ω .	۷	⋖	
-	_+_		AAB B	AABA A A B CACA B BBCF	A ABFCB BCICDE FC FBIDA	A A ABFCB BADBA/ ACA BCICDBECABAB BBCFC FBIDACECC A	88 88 8	4 4 4 4	O V	AA AA A A CI CAB A	AA AA BAA 7 A CB AA C CAB AAA C	4 28 ₹3	4 4 4		
0	_+_	AAB B AB A B B	∢ m	AAACE ACAGE B CBD	BABHE ECCEE IE FBF	AAACEBABHBGECHB A AA A ACAGEECCEEHEBDBD A A AAB CBDE FBFBBCBDBBBBBA	A AA O A BOBBBB	A A B	AAA AB B BA	8448 4 A B	A P P P P P P P P P P P P P P P P P P P	484 88 88	C A A	V V	
7	+-	AAA A A A	⋖	BBDCA A AD CB B	BDCAGBDDEEAAC A ADEEEECDAE CB BACCCGBC	BBDBDCAGBDDEEAACAB AA BAA A ADEEECDAE BAA BAAA A CB BACCCGBC BB A	AB AA BA Baa baaa Bb a	BAA AA A	A A B		88.8	A AB A	4 4 4 4 4		
-2	+_	⋖	AA	ď	B ABGC	A B ABGCAACC BC CCA A B A AAB DA A	A A B A A	∢ ⁴	4	C AA AB AAAB	BA AAA	4	∢	∢	
و	_+-		∢		AA ABAA B	A A B B A A B A A		∢	⋖	ပ	4 4				
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	+0	2	4	9	88	10	12	14	16	18	20	22	24-	26	!
							PSO	PSORICLD							

1 OBS HAD MISSING VALUES

NOTE:

24 PROC PLOT DATA = CRC.DMRGLMB; 25 TITLE4 'OBSERVED & RESIDUALS VS. FITTED RESULTS - COLD TWD';

NOTE: THE PROCEDURE PLOT USED 0.23 SECONDS AND 400K AND PRINTED PAGES 10 TO 11.
NOTE: SAS USED 464K MEMORY.

26 PLOT (SQRTCOLD RSQRTCLD) *PSQRTCLD;

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27511, U.S.A.
                                                                                                                                                                                                                                                                                                                                       TITLE1 'CRC 1988 DRIVEABILITY STUDY - ALTITUDE & OXYGENATE EFFECTS';
TITLE2 'ANALYSIS FOR FUEL, SITE EFFECTS, ETC.;
TITLE3 'THIRD PASS AT GLM';
PROC GLM DATA=CRC.DMRANALY;
CLASS VEHGRP SITE VEHICLE DXY VOLATIL;
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    19 LSMEANS SITE /PDIFF E=SITE*VEHICLE(VEHGRP);
20 LSMEANS OXY / PDIFF;
21 LSMEANS OXY / PDIFF;
22 LSMEANS VOLATIL / PDIFF E=VCHATIL*VEHICLE(VEHGRP);
22 LSMEANS VEHGRP / PDIFF E=VEHICLE(VEHGRP);
23 DUTPUT OUT=CRC.DMRGLMB P=PSQRTCLD R=RSQRTCLD;
NOTE: THE DATA SET CRC.DMRGLMB HAS 938 OBSERVATIONS AND 66 VARIABLES.
NOTE: THE PROCEDURE GLM USED 6.20 SECONDS AND 464K
AND PRINTED PAGES 1 TO 9.
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                                                                          VERSION = FF SERIAL = 171469 MODEL = 3090
                                                                                                                                                                                                                                                                                               ********************************
                                                                                                                                                                                                                                                                                                                                                                                                                                                                   MODEL SORTCOLD = RUNTEMP RUNTEMP*VEHGRP
                                                                                                                                                                                                                                                SAS- "THIRD" PASS AT GLM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               VOLATIL VOLATIL*VEHICLE(VEHGRP)
                                                                                                                                                                                                                                                                                                                     OPTIONS NOCENTER LINESIZE #80;
                                                                                                                          NOTE: SAS OPTIONS SPECIFIED ARE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    SITE SITE * VEHICLE ( VEHGRP )
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 / SS4 SOLUTION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            VEHICLE (VEHGRP)
                                                                                                                                                   LEAVE=0
                                                                          NOTE: CPUID
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   NOTE:
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